

New frequency domain features in LS-DYNA®

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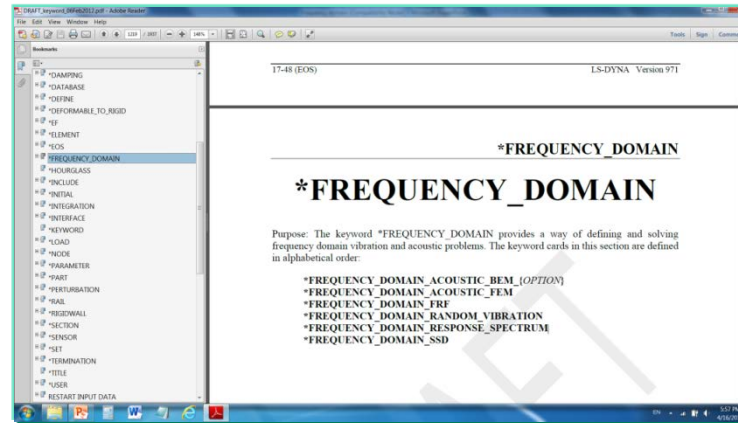
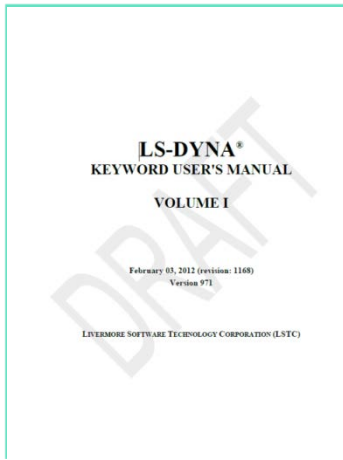
Outline

- Introduction
- Frequency response functions
- Steady state dynamics
- Random vibration & fatigue
- Response spectrum analysis
- Acoustic analysis by BEM/FEM
- Conclusion & future work

1. introduction

Keywords for frequency domain analysis

- FREQUENCY_DOMAIN_FRF
- FREQUENCY_DOMAIN_SSD
- FREQUENCY_DOMAIN_RANDOM_VIBRATION_{OPTION}
- FREQUENCY_DOMAIN_ACOUSTIC_BEM_{OPTION}
- FREQUENCY_DOMAIN_ACOUSTIC_FEM
- FREQUENCY_DOMAIN_RESPONSE_SPECTRUM



Frequency domain vs. time domain

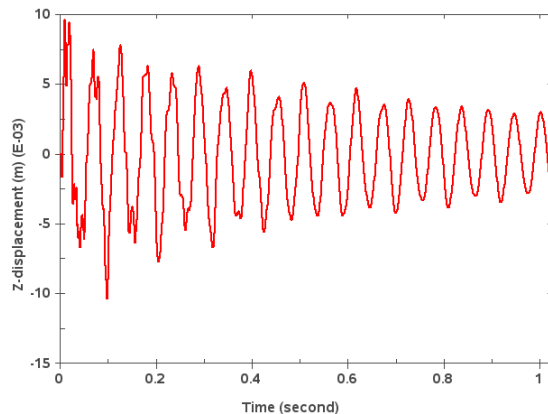
- A time-domain graph shows how a signal changes over time
- A frequency-domain graph shows the distribution of the energy (magnitude, etc.) of a signal over a range of frequencies

Frequency domain analysis

- ✓ Harmonic, periodic loading
- ✓ Resonance
- ✓ Linear dynamics
- ✓ Long history (fatigue testing)
- ✓ Non-deterministic load (random analysis)

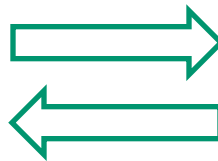
Time domain analysis

- ✓ Transient analysis (penetration)
- ✓ Impact (crash simulation)
- ✓ Large deformation
- ✓ Non-linearity (fracture, contact)

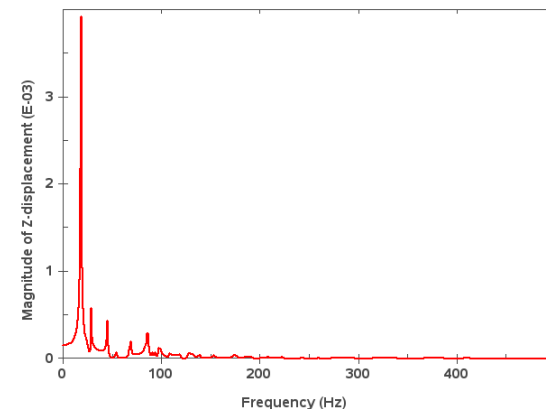


Time domain

Fourier Transform



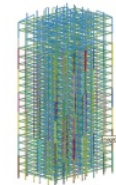
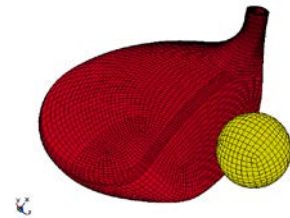
Inverse Fourier Transform



Frequency domain

Application of frequency domain features

- ✓ Vehicle NVH
 - *Interior noise*
 - *Exterior radiated noise*
 - *Vibration*
- ✓ Vehicle Durability
 - *Cumulative damage ratio*
 - *Expected life (mileage)*
- ✓ Aircraft / rocket / spacecraft vibro-acoustics
- ✓ Durability analysis of machines and electronic devices
- ✓ Acoustic design of sports products
- ✓ Civil Engineering
 - *Architectural acoustics (auditorium, concert hall)*
 - *Earthquake resistance*
- ✓ Off-shore platforms, wind turbine, etc.
 - *Random vibration*
 - *Random fatigue*



New databases in frequency domain

- BINARY databases

Keyword ***DATABASE_FREQUENCY_BINARY_{OPTION}**

Database	Isocode	used for
D3SSD	21	Steady state dynamics
D3SPCM	22	Response spectrum analysis
D3PSD	23	Random vibration PSD
D3RMS	24	Random vibration RMS
D3FTG	25	Random vibration fatigue
D3ACS	26	FEM acoustics
D3ATV	27	BEM acoustic transfer vector

- ASCII databases

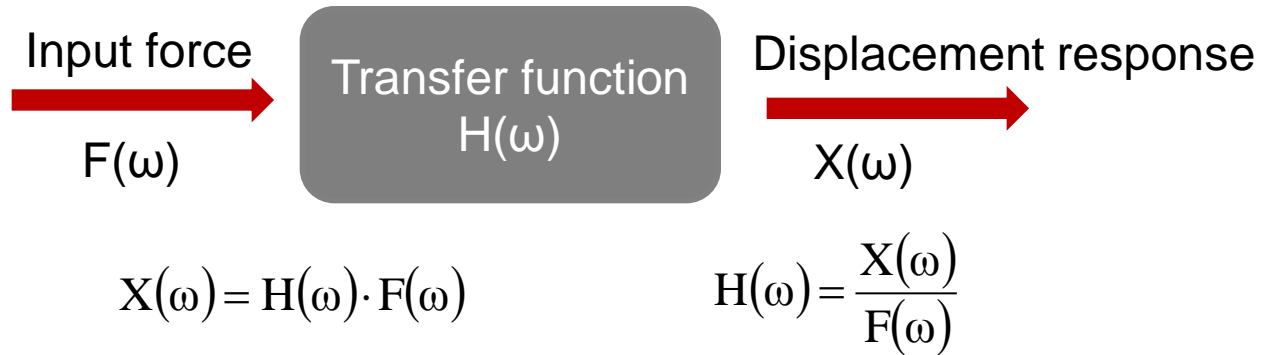
- ✓ FRF: frf_amplitude, frf_angle, frf_real, frf_imag
- ✓ BEM acoustics: Press_Pa, Press_dB, bepres, fringe_*, panel_contribution_NID,
- ✓ SSD: elout_ssd, nodout_ssd, ...

Accessible to LS-PREPOST !



2. Frequency response function

Introduction: frf



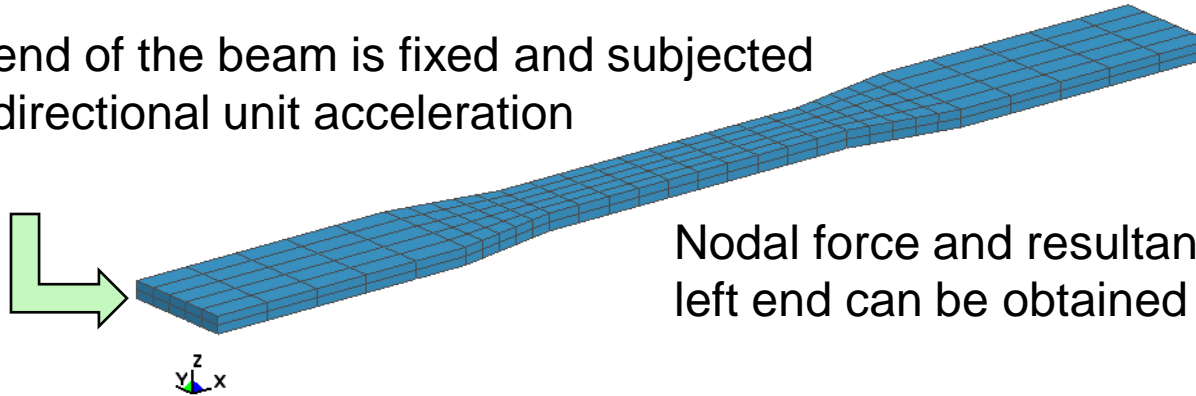
- Foundation of modern experimental system analysis and experimental modal analysis
- Expresses structural response due to unit load as a function of frequency
- property of structure system
- complex function, with real / imaginary components, or magnitude / phase angle pairs
- Efficient restart based on modal analysis results
- Important application in transfer path analysis

FRF formulations

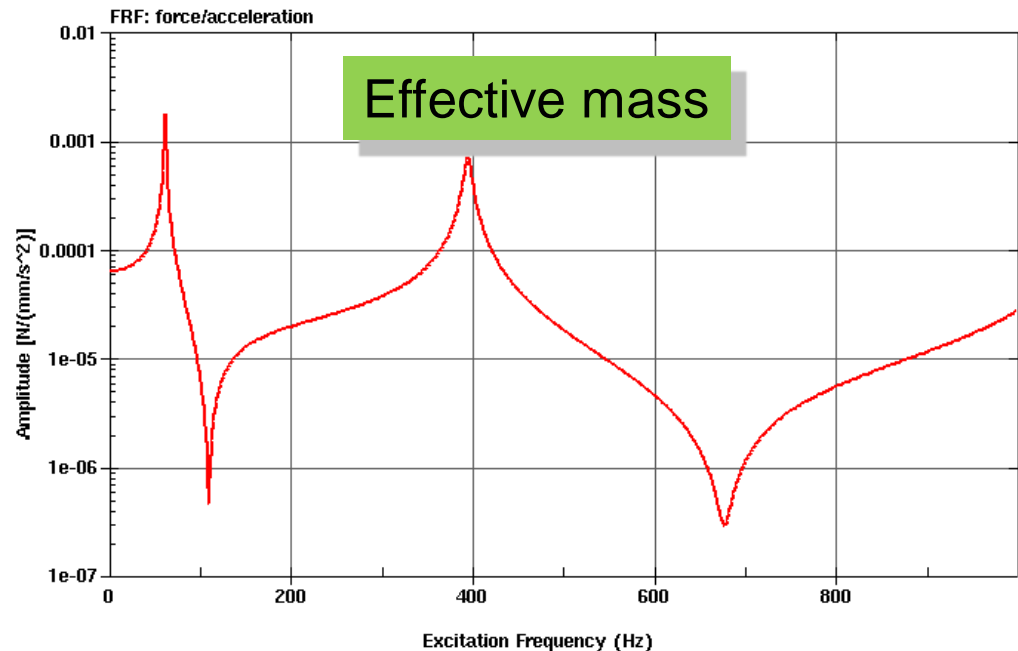
Accelerance, Inertance	$\frac{\text{Acceleration}}{\text{Force}}$
Effective Mass	$\frac{\text{Force}}{\text{Acceleration}}$
Mobility	$\frac{\text{Velocity}}{\text{Force}}$
Impedance	$\frac{\text{Force}}{\text{Velocity}}$
Dynamic Compliance, Admittance, Receptance	$\frac{\text{Displacement}}{\text{Force}}$
Dynamic Stiffness	$\frac{\text{Force}}{\text{Displacement}}$

Nodal force/resultant force for a beam model

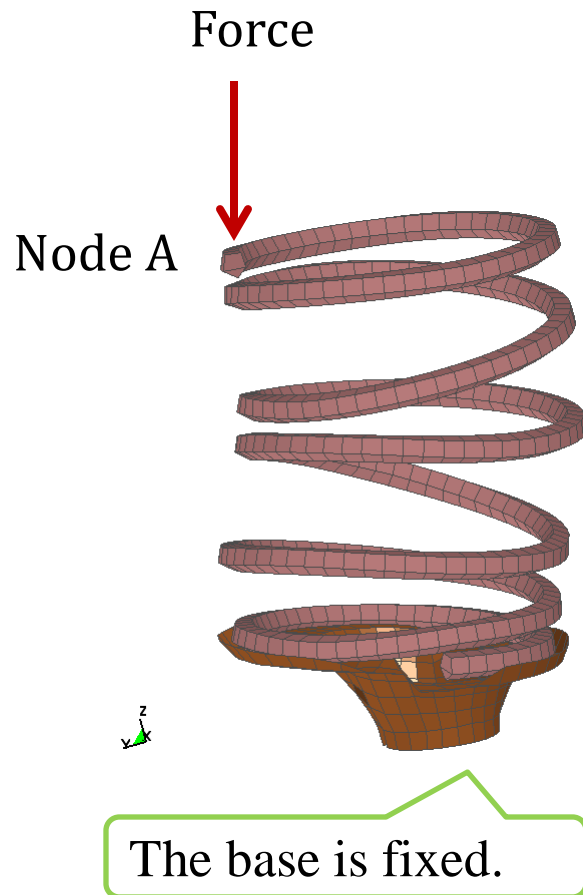
Left end of the beam is fixed and subjected to z-directional unit acceleration



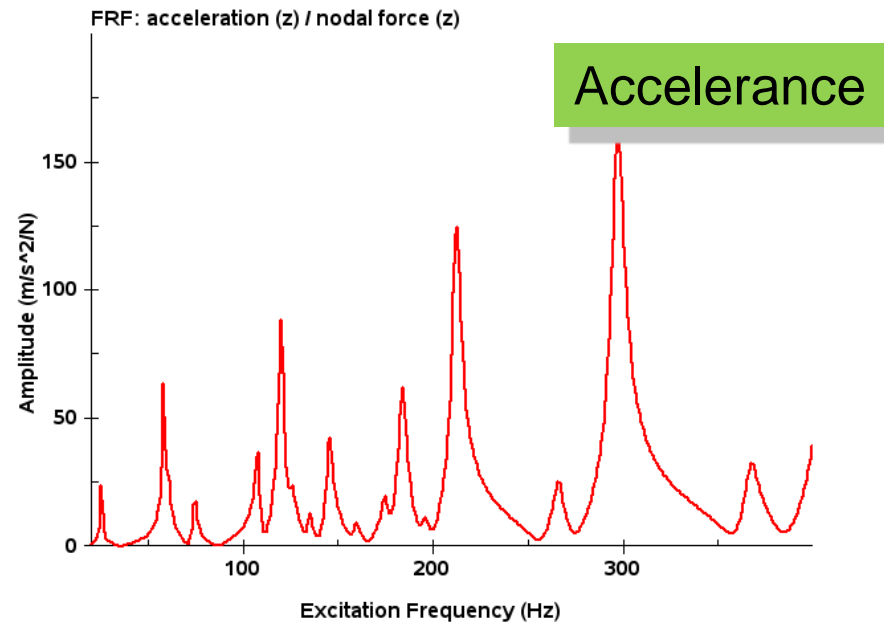
Nodal force and resultant force FRF at the left end can be obtained



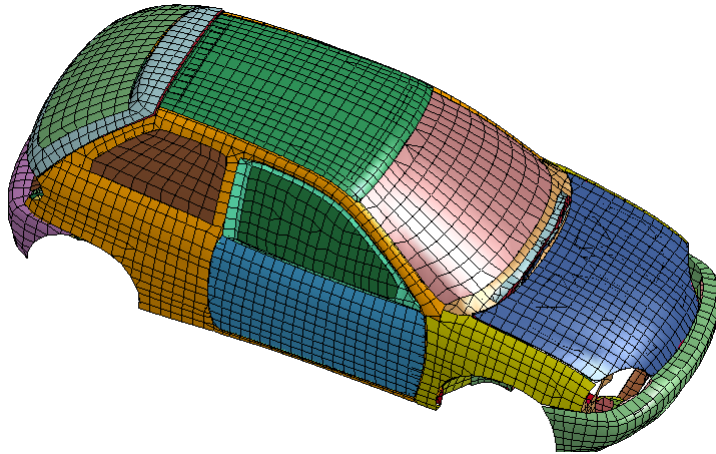
FRF for a spring in suspension system



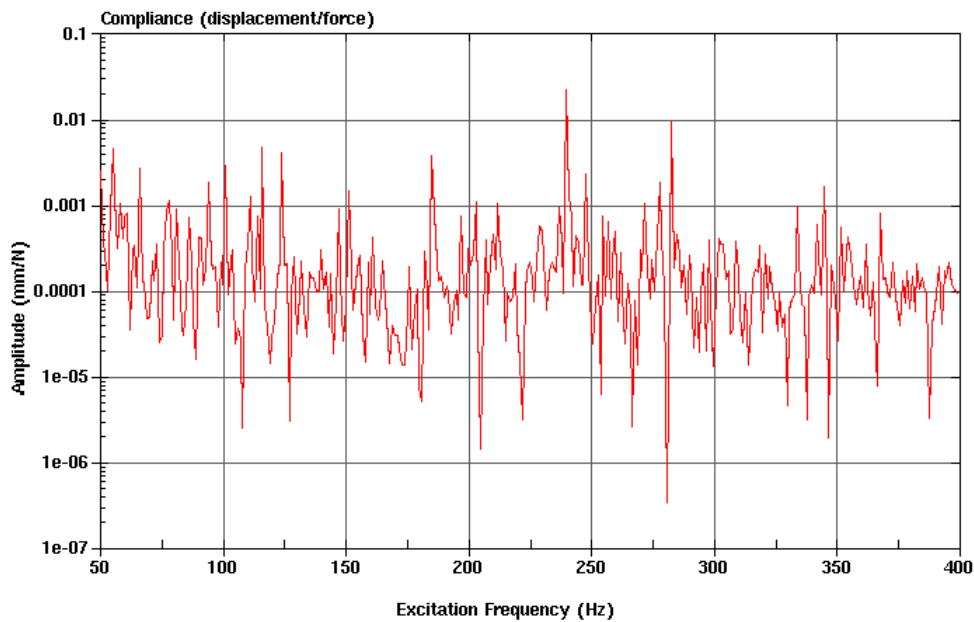
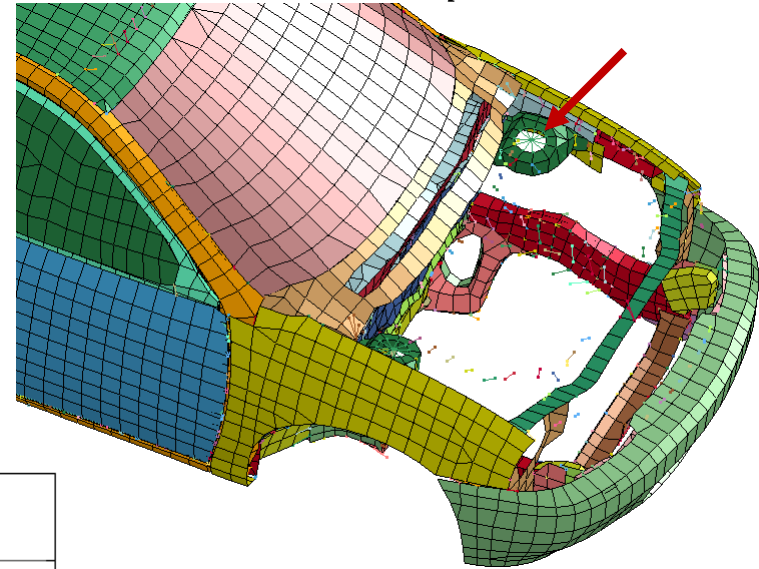
Point FRF at node A is computed
 $FRF = \text{acceleration} / \text{nodal force}$



FRF for a simplified car body



Nodal force applied and displacement measured

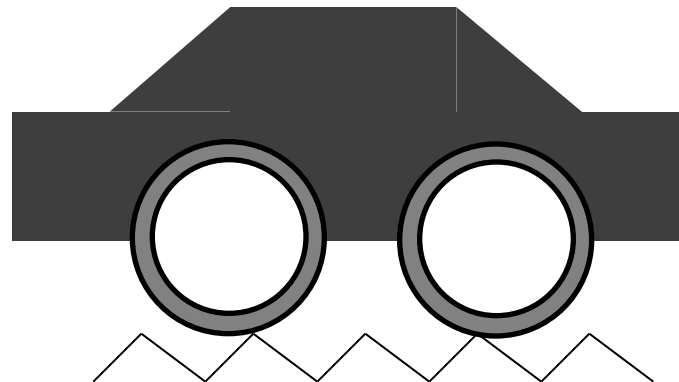


Dynamic compliance

3. Steady state dynamics

Introduction: SSD

- *Harmonic excitation* is often encountered in engineering systems. It is commonly produced by the unbalance in rotating machinery.
- The load may also come from periodical load, e.g. in fatigue test.
- The excitation may also come from uneven base, e.g. the force on tires running on a zig-zag road.
- Both input and output are given as complex variables (e.g. amplitude / phase angle pairs)
- Based on modal approach (modal analysis is performed first)
- May be called as
 - Harmonic vibration
 - Steady state vibration
 - Steady state dynamics

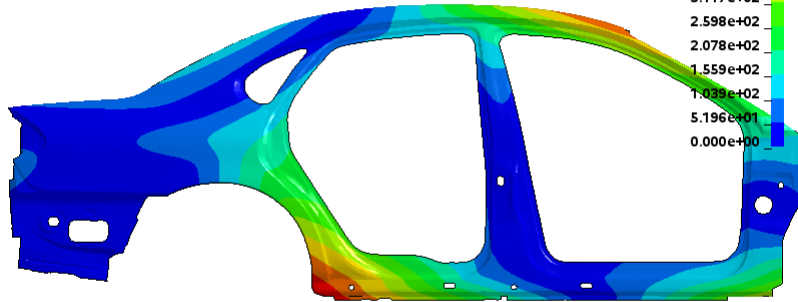


Acceleration SSD for body frame

Freq = 10
Contours of Y-acceleration
min=0, at node# 2348800
max=519.557, at node# 2361762

Fringe Levels

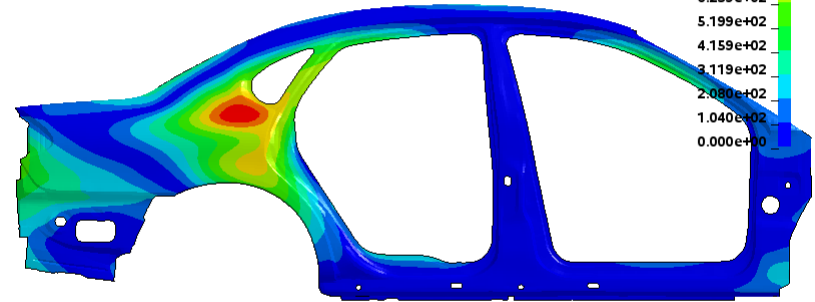
5.196e+02
4.676e+02
4.156e+02
3.637e+02
3.117e+02
2.598e+02
2.078e+02
1.559e+02
1.039e+02
5.196e+01
0.000e+00



Freq = 60
Contours of Y-acceleration
min=0, at node# 2348800
max=1039.79, at node# 2359759

Fringe Levels

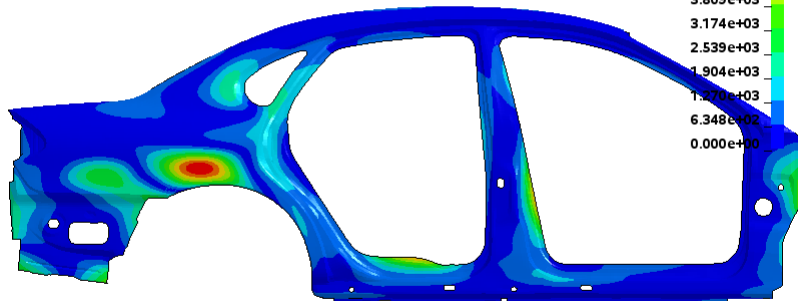
1.040e+03
9.358e+02
8.318e+02
7.279e+02
6.239e+02
5.199e+02
4.159e+02
3.119e+02
2.080e+02
1.040e+02
0.000e+00



Freq = 110
Contours of Y-acceleration
min=0, at node# 2348800
max=6347.77, at node# 2360071

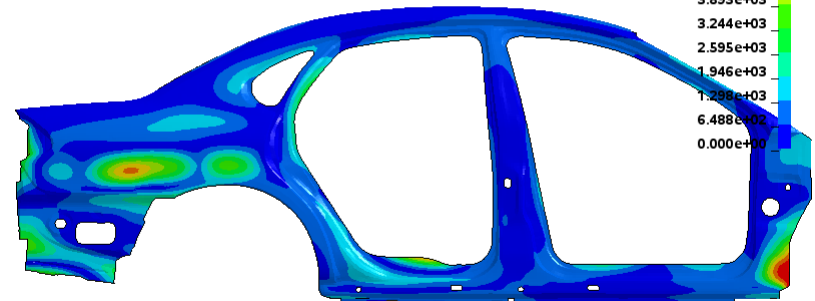
Fringe Levels

6.348e+03
5.713e+03
5.078e+03
4.443e+03
3.809e+03
3.174e+03
2.539e+03
1.904e+03
1.270e+03
6.348e+02
0.000e+00



Z
L X

5.190e+03
4.541e+03
3.893e+03
3.244e+03
2.595e+03
1.946e+03
1.298e+03
6.488e+02
0.000e+00



(given by d3ssd)

4. Random vibration & fatigue

Introduction: random vibration

Why we need random vibration analysis?

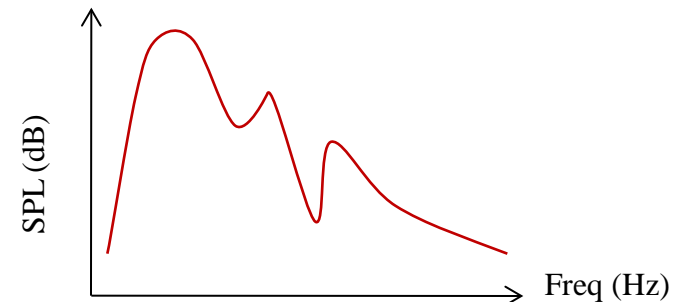
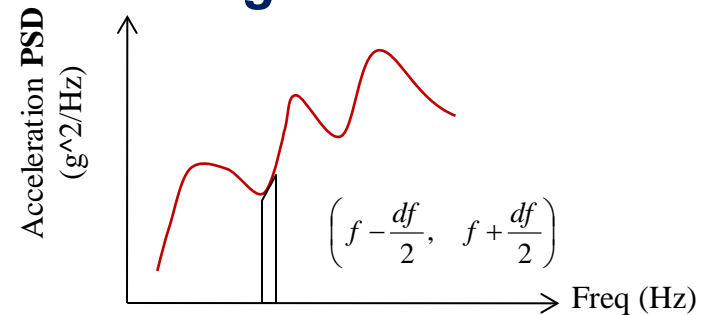
- In many cases, the loading on a structure is undeterministic
- Many vibration environments are not related to a specific driving frequency (may have input from multiple sources)
- Provide input data for random fatigue and durability analysis

Examples

- Fatigue
- Wind-turbine
- Air flow over a wing or past a car body
- Acoustic input from jet engine exhaust
- Earthquake ground motion
- Wheels running over a rough road
- Ocean wave loads on offshore platforms

Based on Boeing's N-FEARA package

Loading: PSD or SPL

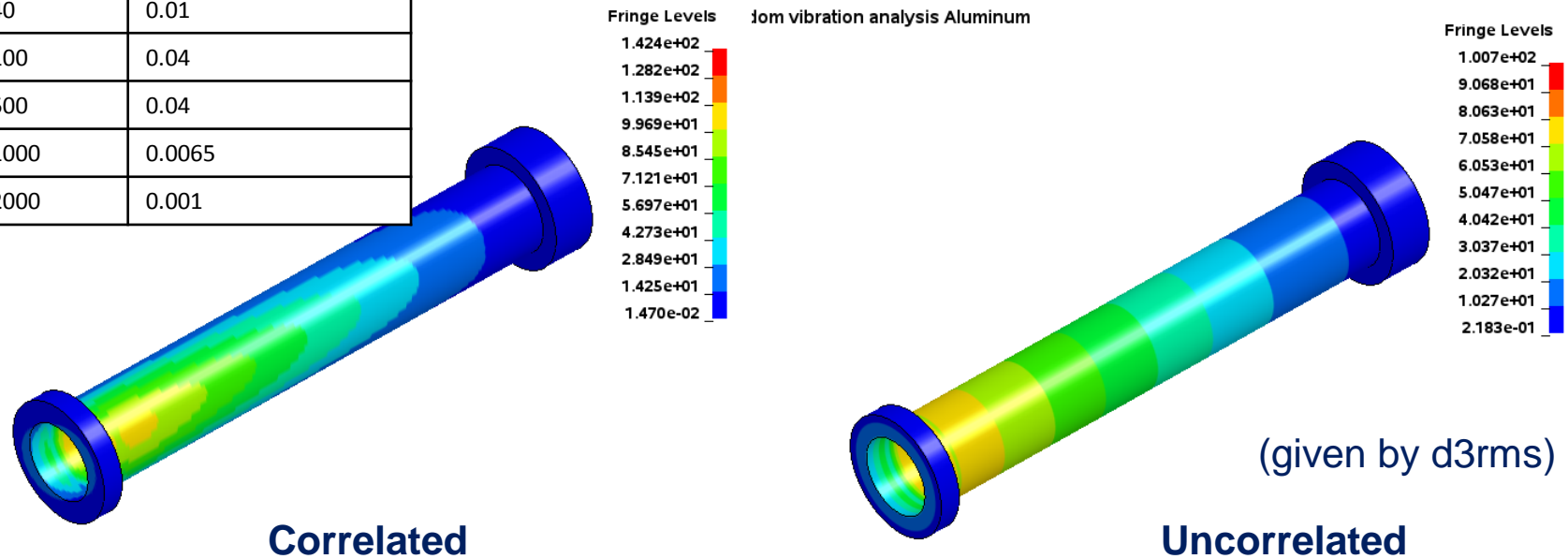


A pipe under base acceleration

The model is a simple pipe with 83700 elements and 105480 nodes. It is subjected to base acceleration PSD 1) in x, y and z-directions correlated; 2) in x, y and z-directions uncorrelated.

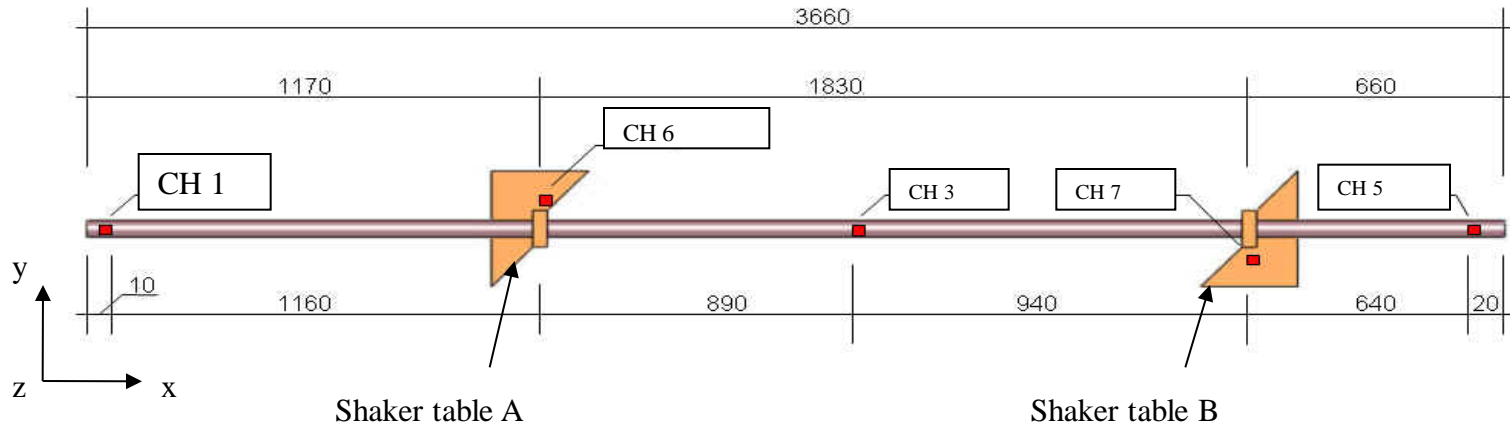
F (Hz)	Acce. Psd (g ² /Hz)
5	0.01
40	0.01
100	0.04
500	0.04
1000	0.0065
2000	0.001

RMS of Von Mises stress



Max Von Mises RMS stress (MPa)	
Correlated	Uncorrelated
142.4	100.7

Shaker table test



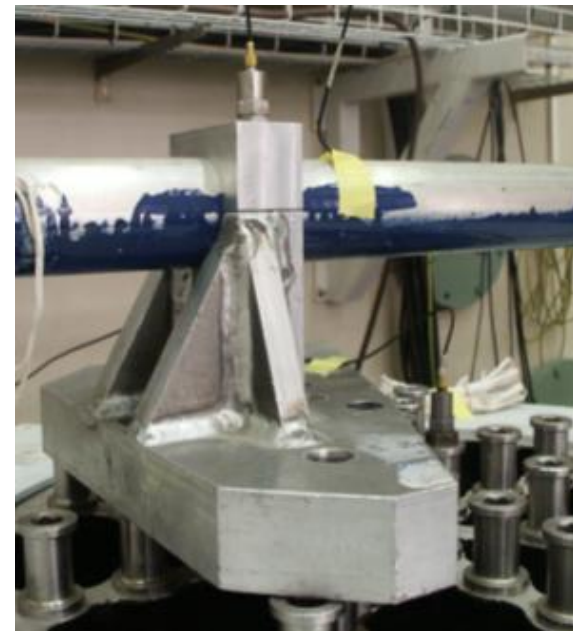
Tube thickness = 3.3 mm

The tube was fixed to the shaker tables using aluminum blocks which surrounded the tube and were tightened using screws.

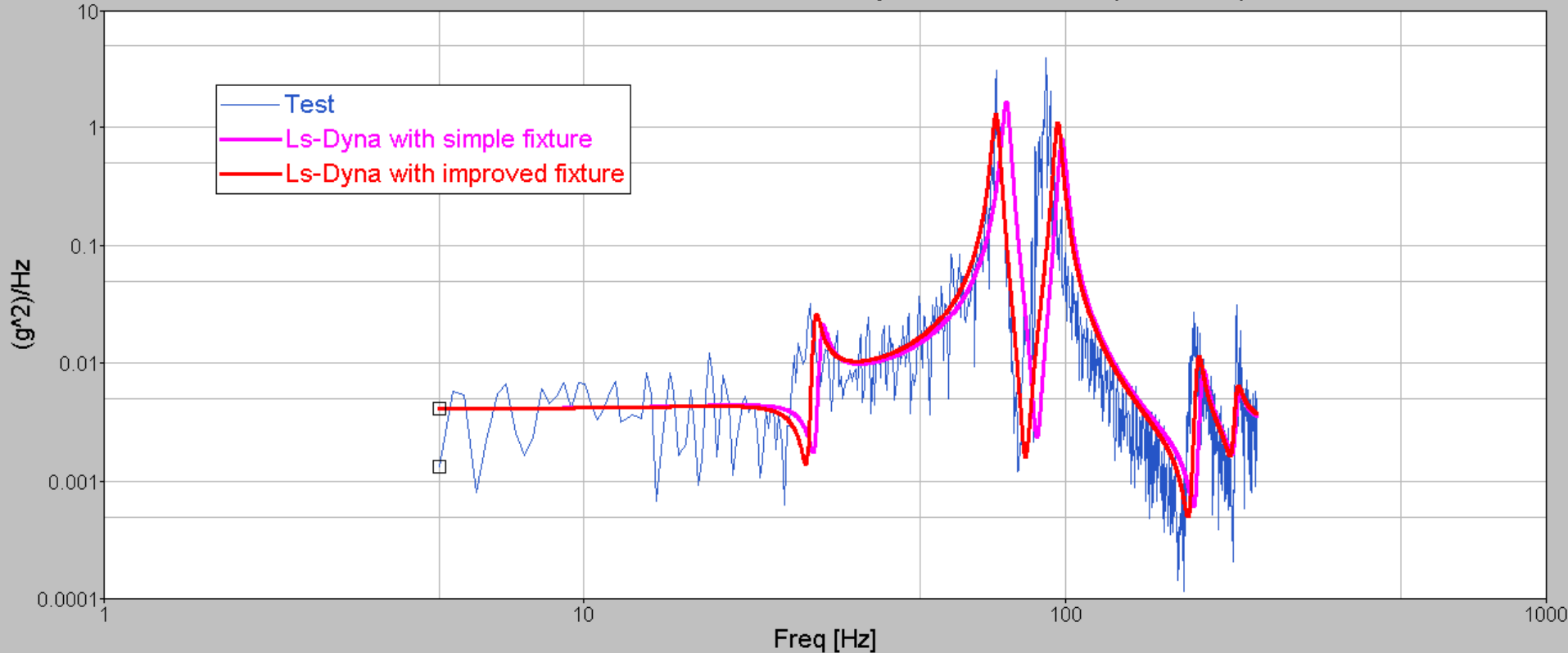
Base acceleration PSD load

Total: 1.00 [Grms]

No.	Freq.	g^2/Hz
1	5	0.004082
2	250	0.004082



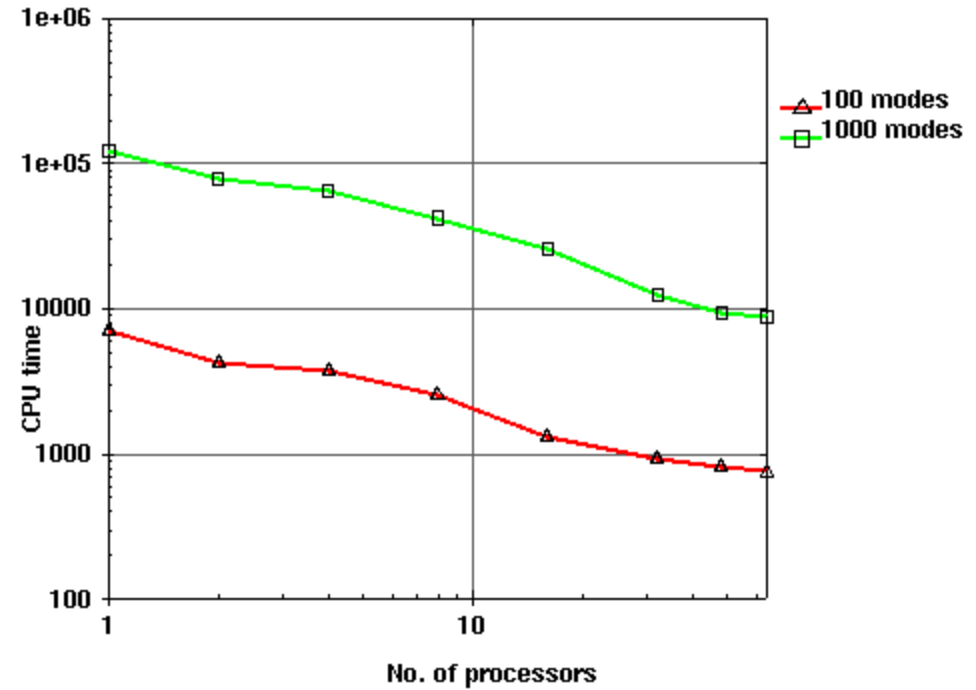
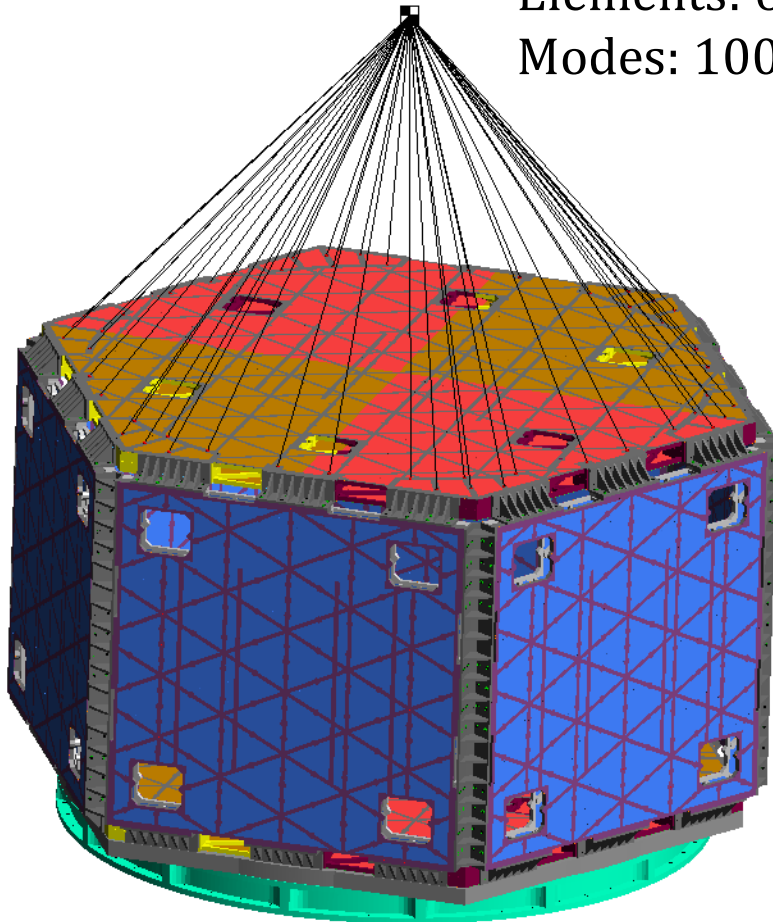
PSD of acceleration - CH 3 - Test results vrs. Ls-Dyna results with simple and improved fixture



Ofir Shor, Yoav Lev, Yun Huang, *Simulation of a Thin Walled Aluminum Tube Subjected to Base Acceleration Using LS-DYNA's Vibro-Acoustic Solver*, 11th International LS-DYNA Users' Conference, Dearborn, MI, 2010.

MPP random vibration analysis

Nodes: 800k
Elements: 660k
Modes: 1000



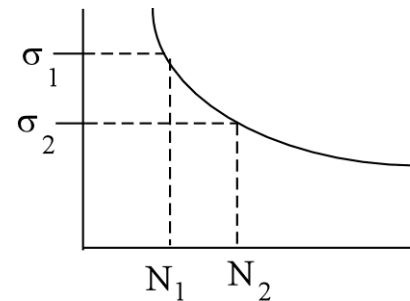
Introduction: random vibration fatigue

*FREQUENCY_DOMAIN_RANDOM_VIBRATION_FATIGUE

- Calculate fatigue life of structures under random vibration
- Based on S-N fatigue curve
- Based on probability distribution & Miner's Rule of Cumulative Damage Ratio

$$R = \sum_i \frac{n_i}{N_i}$$

- Schemes:
 - ✓ *Steinberg's Three-band technique*
 - ✓ *Dirlik method*
 - ✓ *Narrow band method*
 - ✓ *Wirsching method*
 - ✓ ...



Typical SN (or Wöhler) curve

S-N fatigue curve definition

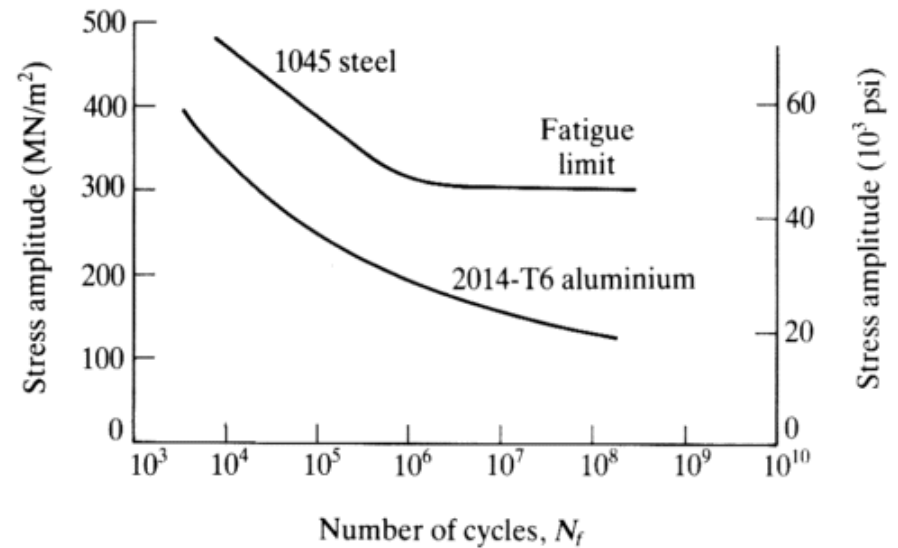
- By *define_curve
- By equation

$$N \cdot S^m = a$$

$$\log(S) = a - b \cdot \log(N)$$

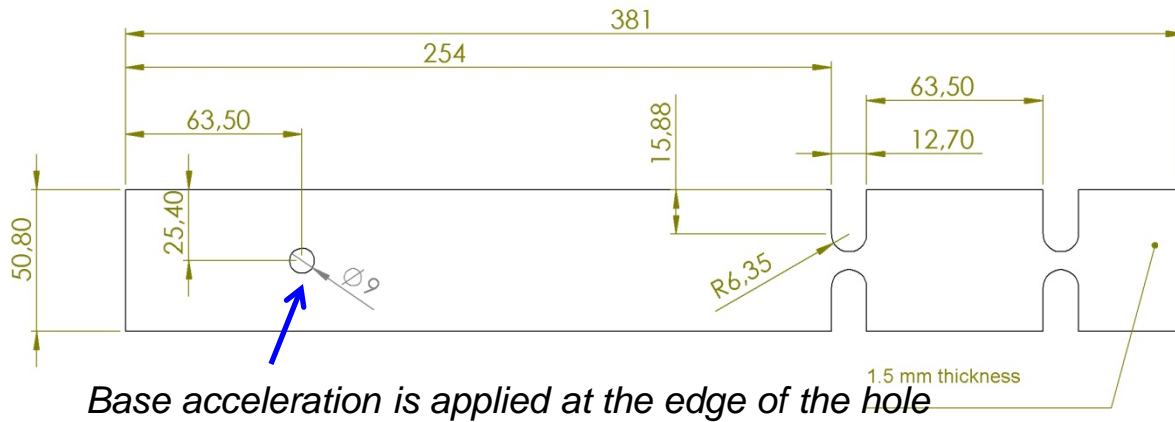
N: number of cycles for fatigue failure

S: stress



Source of picture: <http://www.efunda.com>

A beam with pre-defined notch

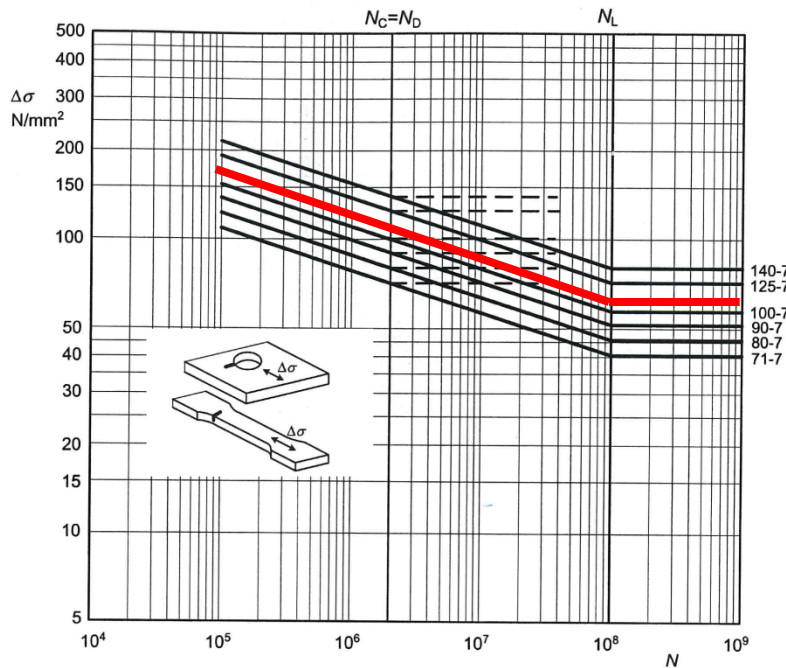


Aluminum alloy 5754

$$\rho = 2700 \text{ Kg/m}^3$$

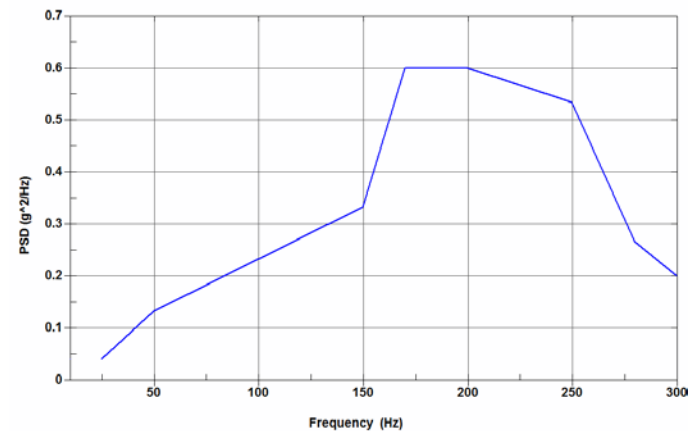
$$E = 70,000 \text{ MPa}$$

$$\nu = 0.33$$

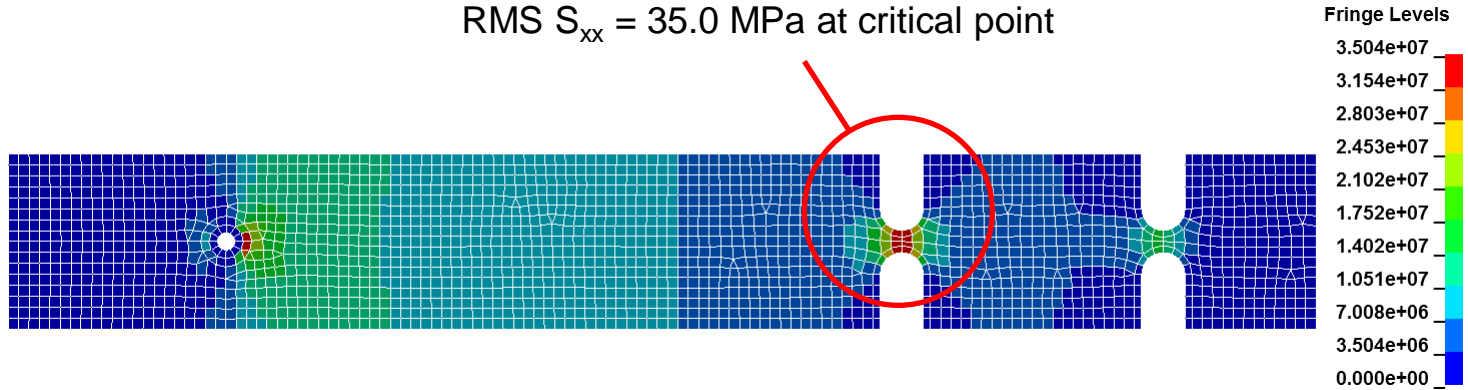


Acceleration PSD

(exposure time: 1800 seconds)



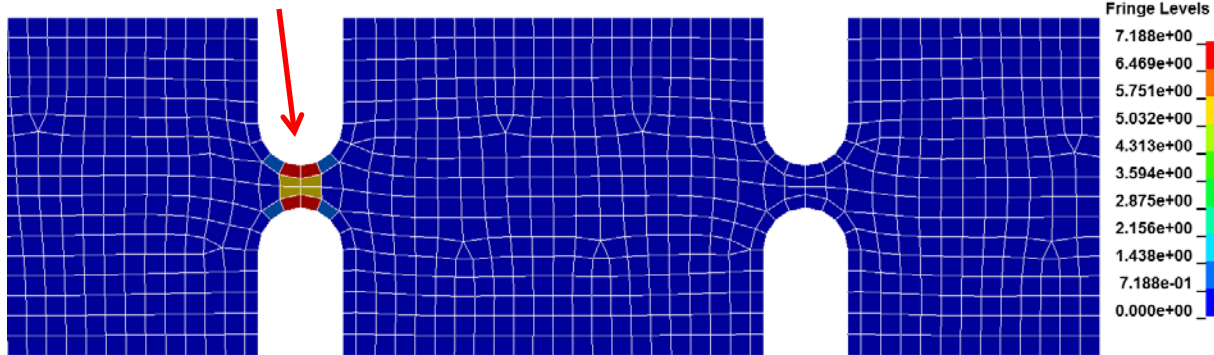
RMS S_{xx} = 35.0 MPa at critical point



Analysis method	Expected life	Damage ratio
Experiment	7mn 25s	-
Steinberg	4mn 10s	7.19
Dirlik	5mn 25s	5.54
Narrow Band	2mn 05s	14.41
Wirsching	5mn 45s	5.08
Chaudhury & Dover	6mn 03s	6.03
Tunna	4mn 06s	7.31
Hancock	22mn 18s	1.35

CODE	RMS S_{xx}
ANSYS	33.5 MPa
RADIOSS® BULK	35.7 MPa
LS-DYNA	35.0 MPa

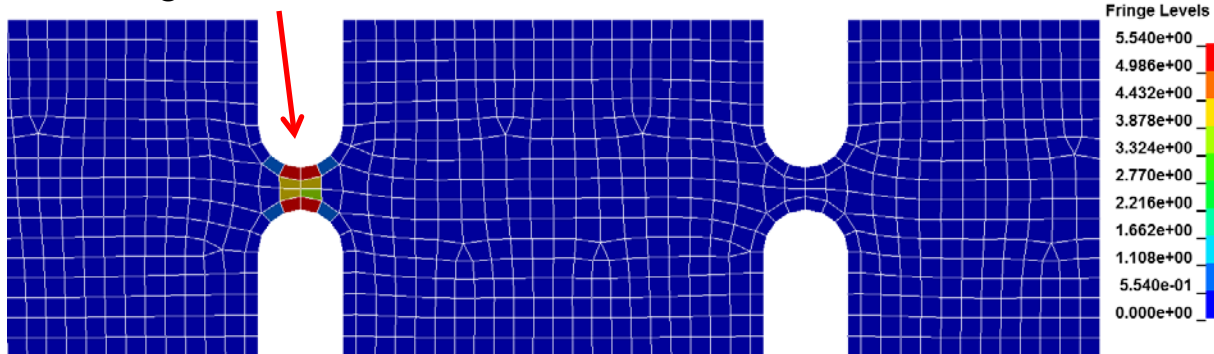
Damage ratio = 7.188



Cumulative damage ratio by Steinberg's method

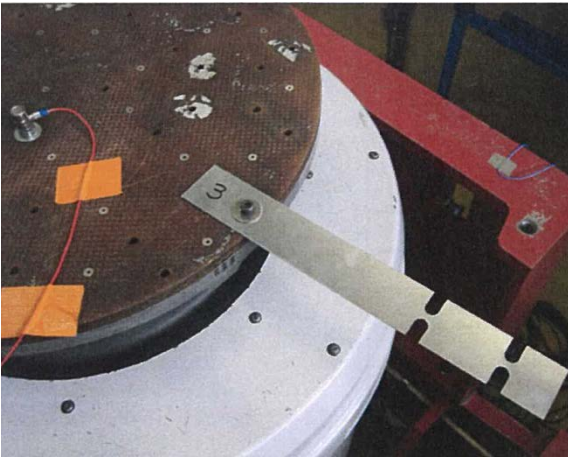
(given by d3ftg)

Damage ratio = 5.540

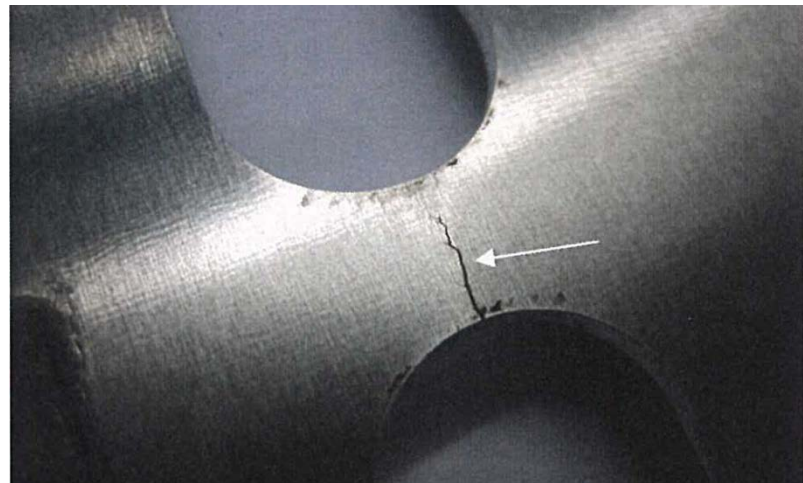


Cumulative damage ratio by Dirlik method

Experiment setup



Failure at the notched point in experiment



How to include pre-existing fatigue damage

*FREQUENCY_DOMAIN_RANDOM_VIBRATION_FATIGUE

Card1	1	2	3	4	5	6	7	8
Variable	MDMIN	MDMAX	FNMIM	FNMAX	RESTRT	MFTG	RESTRM	INFTG
Type	I	I	F	F	I	I	I	I
Default	1		0.0		0	0	0	0

Define Card 7 if option FATIGUE is used and INFTG=1.

Card7	1	2	3	4	5	6	7	8
Variable	FILENAME							
Type	C							
Default	d3ftg							

VARIABLE

DESCRIPTION

INFTG

Flag for including initial damage ratio.
EQ.0: no initial damage ratio,
EQ.1: read existing d3ftg file to get initial damage ratio.

FILENAME

Path and name of existing binary database (by default, D3FTG) for initial damage ratio.

Regarding fatigue life for stress below last pt on SN curve

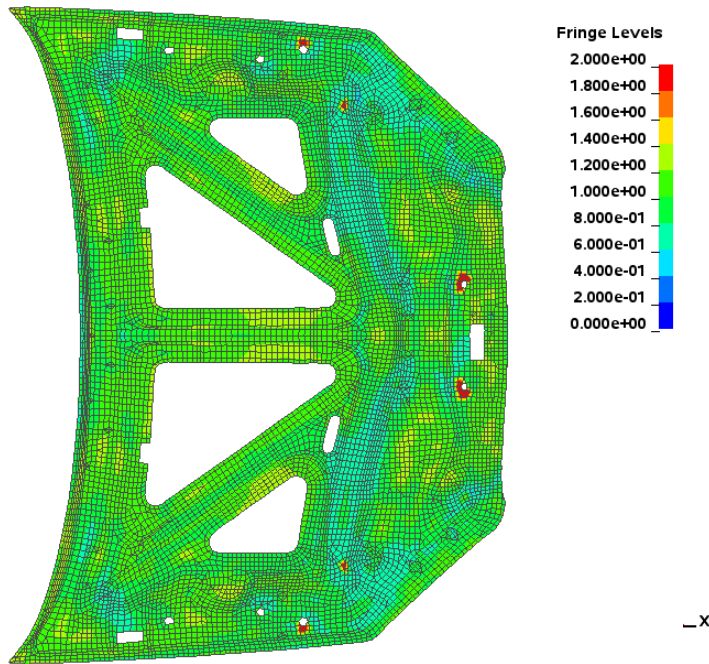
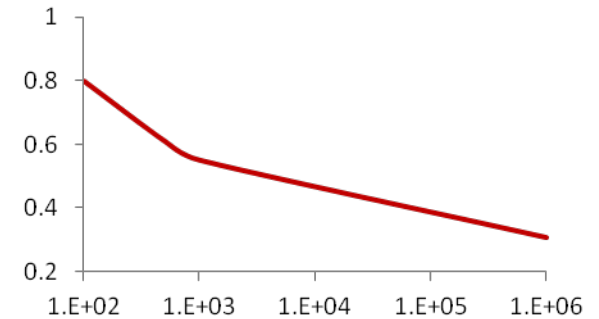
SNLIMT

Fatigue life for stress lower than the lowest stress on S-N curve.

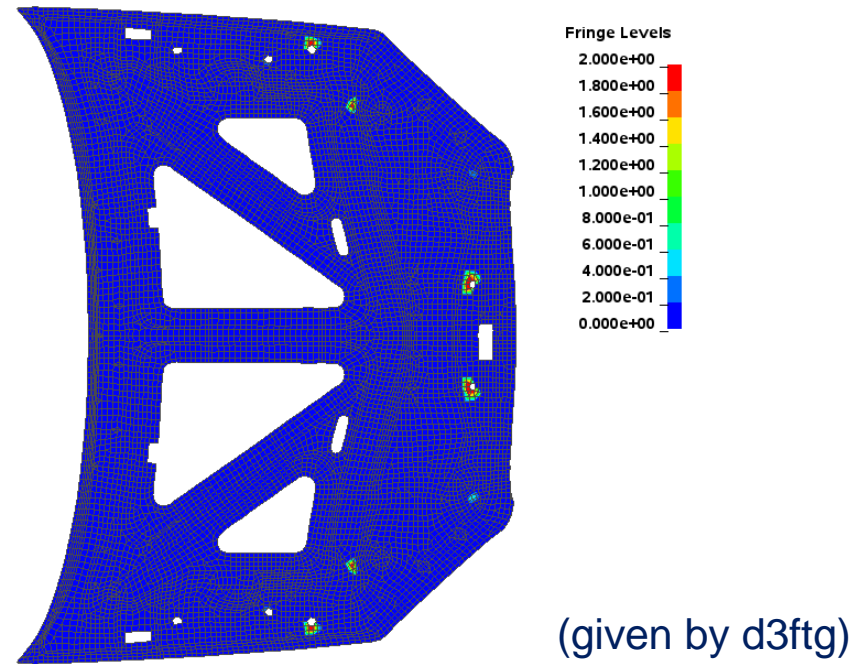
EQ.0: use the life at the last point on S-N curve

EQ.1: extrapolation from the last two points on S-N curve

EQ.2: infinity.

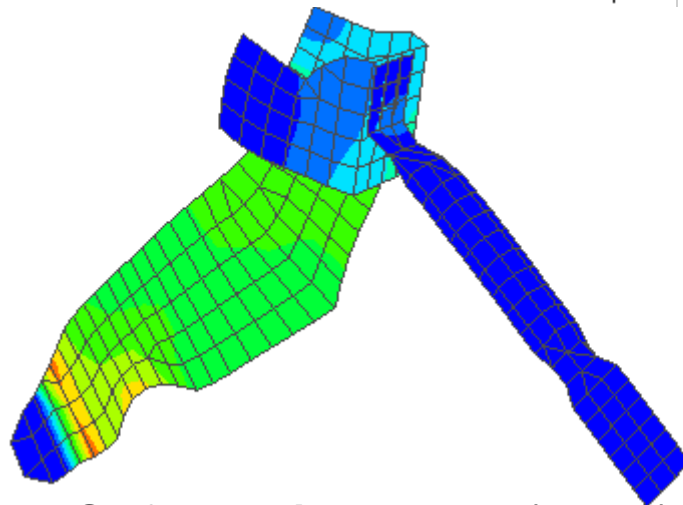
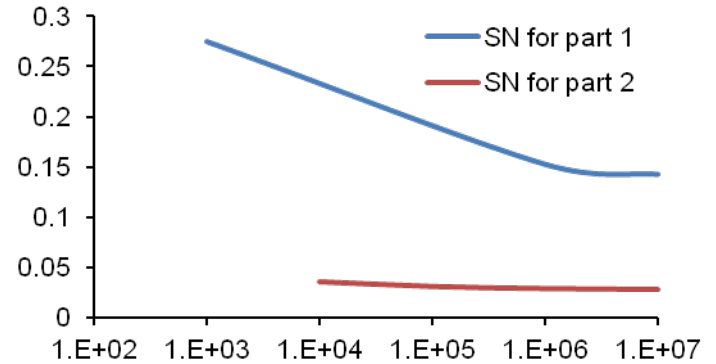
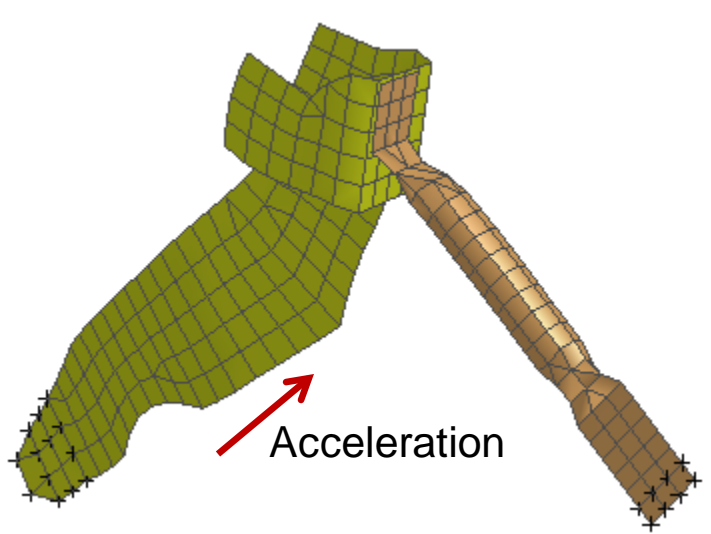


SNLIMT = 0

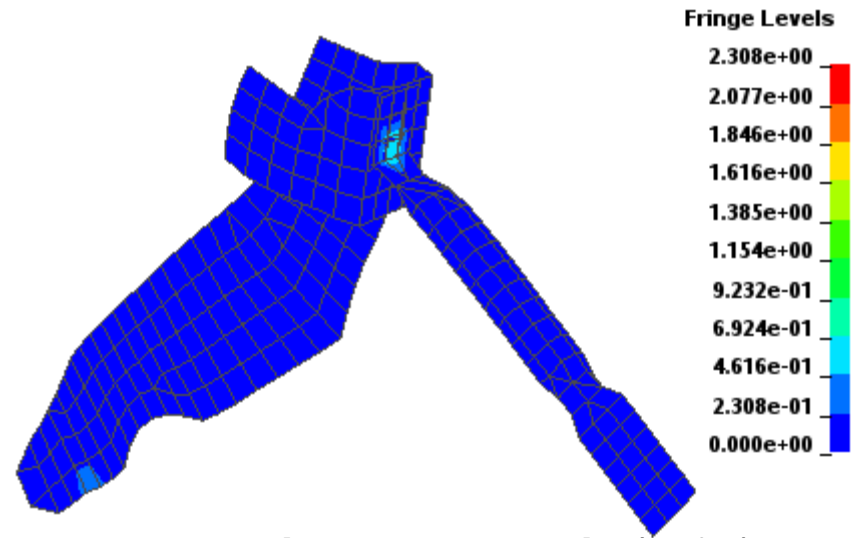


SNLIMT = 2

Example: multi S-N curves in one model



RMS of Von Mises stress (d3rms)



Accumulative damage ratio (d3ftg)

5. Response spectrum analysis

Introduction: response spectrum analysis

*FREQUENCY_DOMAIN_RESPONSE_SPECTRUM

- Use various mode combination methods to evaluate peak response of structure due to input spectrum.
- The input spectrum is the peak response (acceleration, velocity or displacement) of single degree freedom system with different natural frequencies.
- The input spectrum is dependent on damping (using ***DEFINE_TABLE** to define the series of excitation spectrum corresponding to each damping ratio).
- Output binary database: d3spcm (accessible by LS-PREPOST).
- It is an approximate method.
- It has important application in *earthquake engineering, nuclear power plants design* etc.

Capabilities

Mode combination

- SRSS method
- NRC Grouping method
- CQC method
- Double Sum methods
 - ✓ Rosenblueth-Elorduy coefficient
 - ✓ Gupta-Cordero coefficient
 - ✓ Modified Gupta-Cordero coefficient
- NRL SUM method
- Rosenblueth method

Input spectrum

- Base velocity
- Base acceleration
- Base displacement
- Nodal force
- Pressure

Frequency interpolation

- Logarithmic
- Semi-logarithmic
- Linear

Results

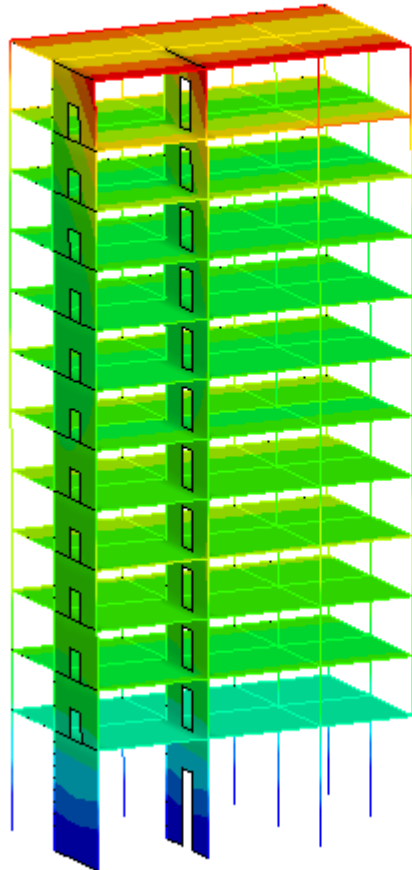
- BINARY plot file: d3spcm
- ASCII files: nodout_spcm, elout_spcm

Applications

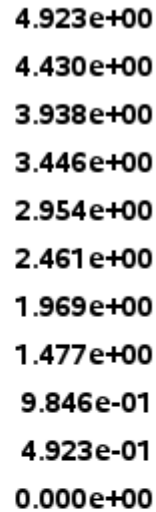
- Civil and hydraulic buildings
 - ✓ Dams
 - ✓ Bridges
 - ✓ High buildings
- Nuclear power plants

Example: multi-story tower

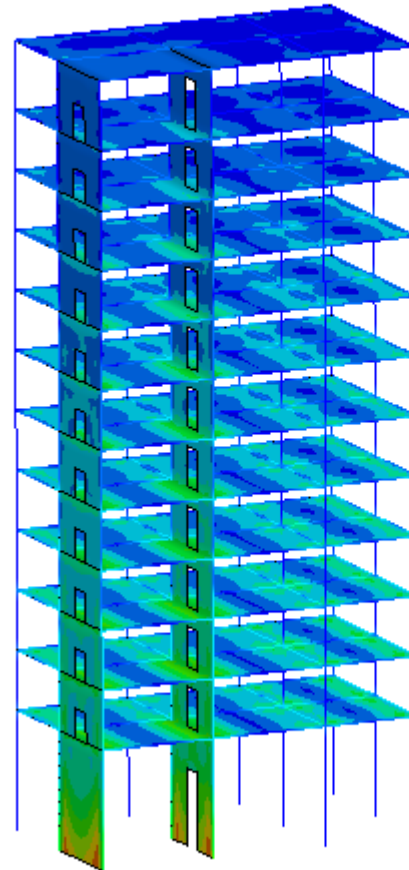
Contours of X-acceleration
 min=0, at node# 1
 max=4.92278, at node# 4082



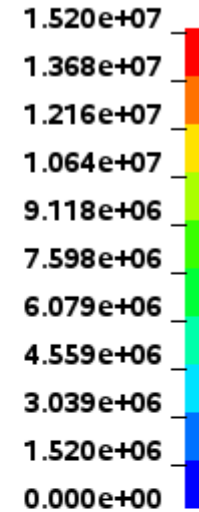
Fringe Levels



Contours of Effective Stress (v-m)
 max IP. value
 min=0, at elem# 1
 max=1.5197e+07, at elem# 2768



Fringe Levels



Loading

X , Y acceleration

Mode combination

SRSS

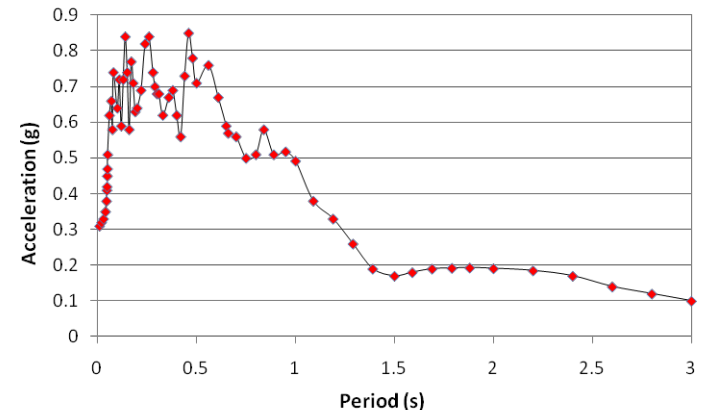
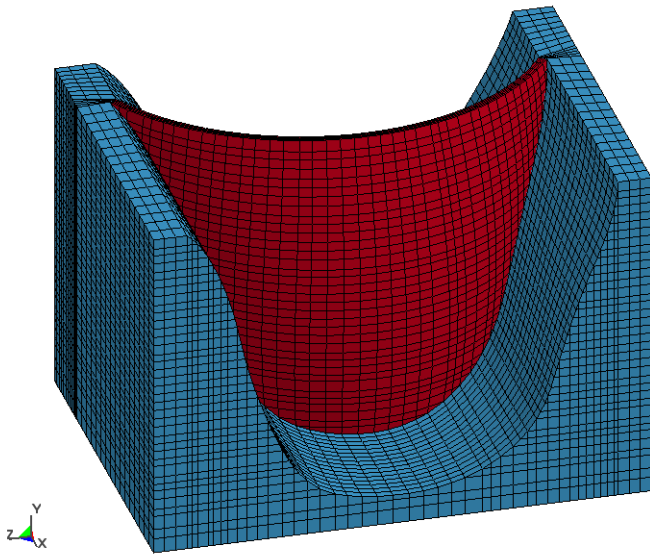


(given by d3spcm)



Example: arch dam

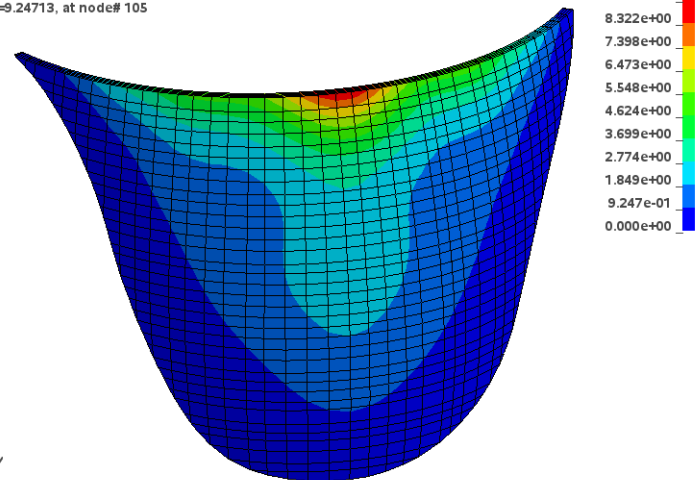
- 464.88 feet high
- Rigid foundation
- Subjected to x-directional ground acceleration spectrum



The pseudo-acceleration spectrum of El Centro earthquake ground motion ($\zeta=5\%$)

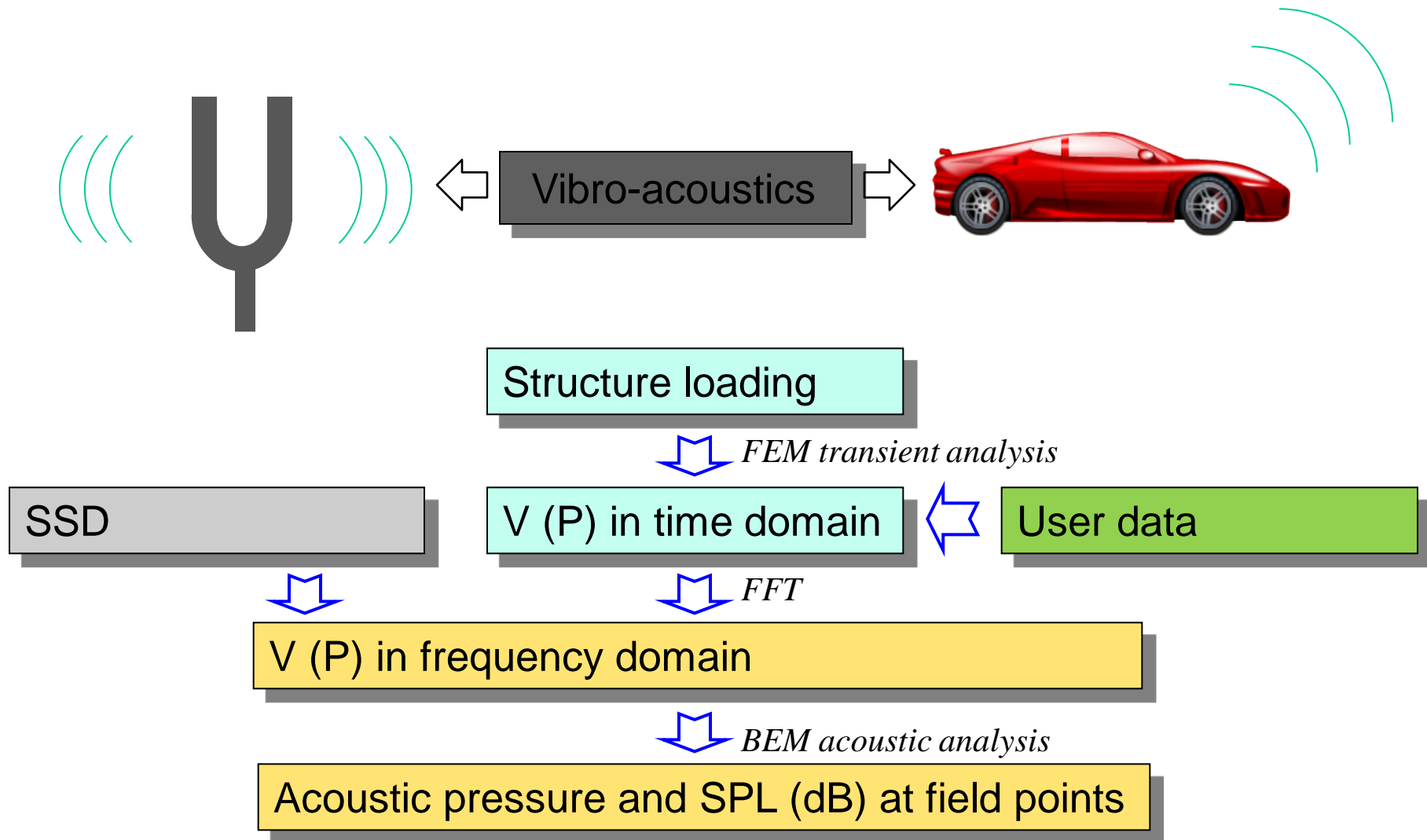
The 1940 El Centro earthquake (or 1940 Imperial Valley earthquake) occurred on May 18 in the Imperial Valley in Southern California near the border of the United States and Mexico. It had a magnitude of 6.9.

Contours of X-acceleration
min=0, at node# 2
max=9.24713, at node# 105



6. Acoustic analysis by BEM/FEM

Introduction: vibro-acoustics



*FREQUENCY_DOMAIN_ACOUSTIC_BEM_{OPTION}

BEM (accurate)

- Indirect variational boundary element method
- Collocation boundary element method

They used to be time consuming

A fast solver based on domain decomposition

MPP version

Approximate (simplified) methods

- Rayleigh method
- Kirchhoff method

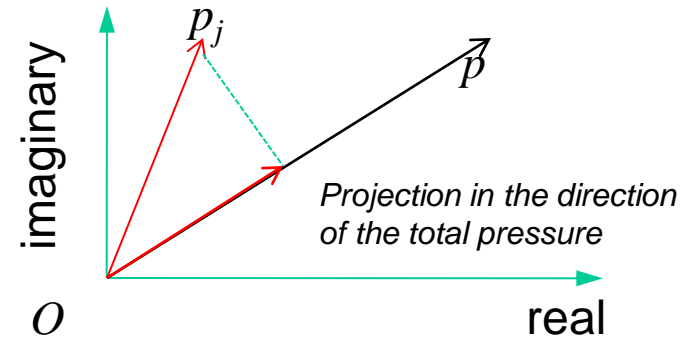
Assumptions and simplification in formulation

Very fast since no equation system to solve

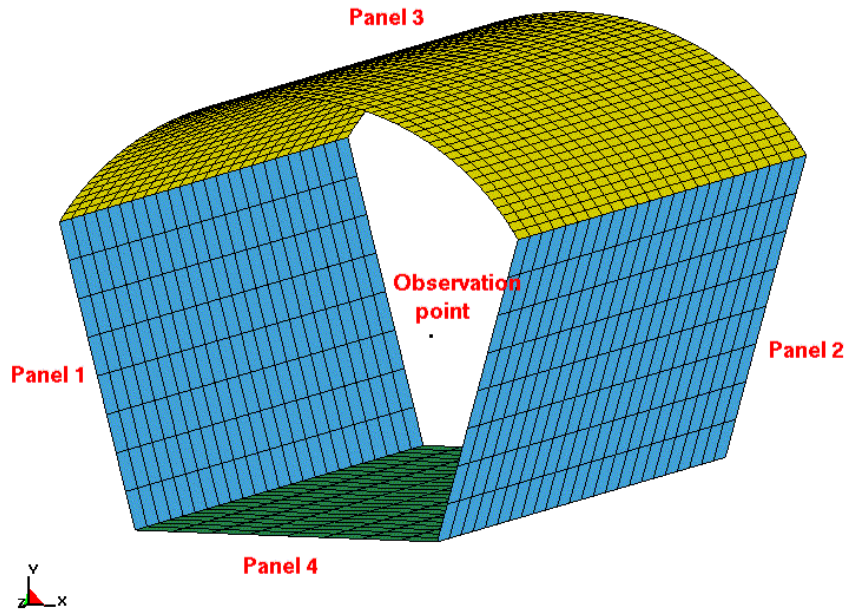
Acoustic panel contribution

$$p(P) = \sum_{j=1}^N \int_{\Gamma_j} \left(G \frac{\partial p}{\partial n} - p \frac{\partial G}{\partial n} \right) d\Gamma_j$$

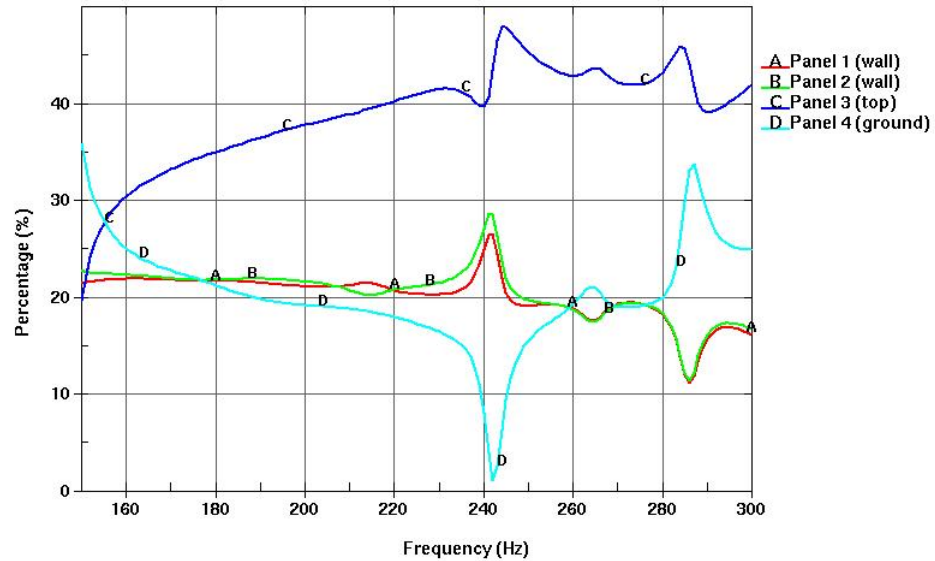
$$= \sum_{j=1}^N p_j(P)$$



A simplified tunnel model

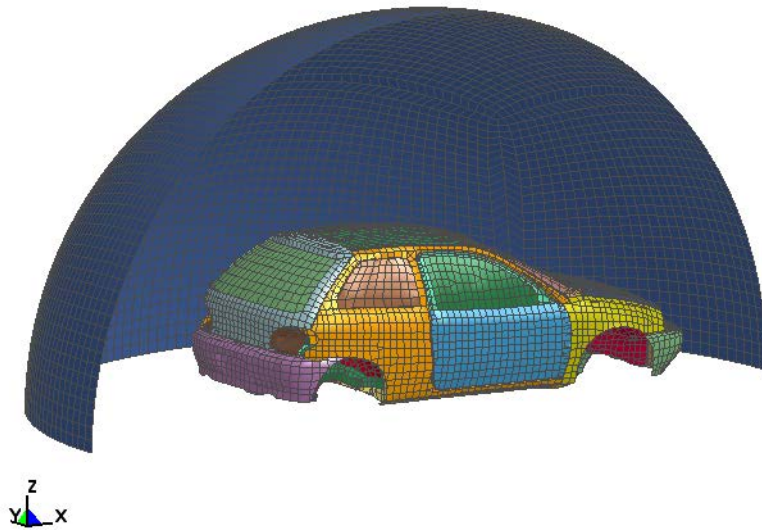


Panel contribution at node 5401

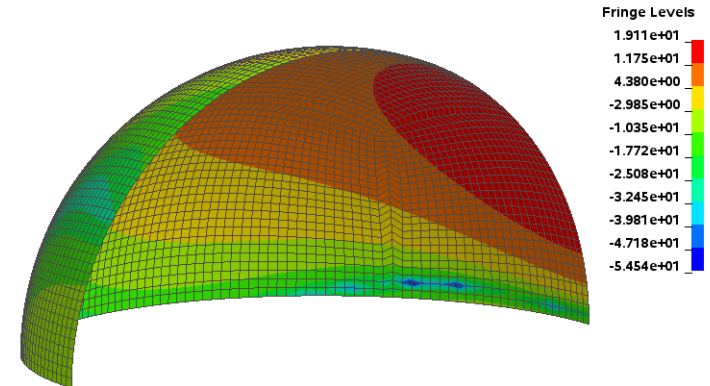


Radiated noise by a car

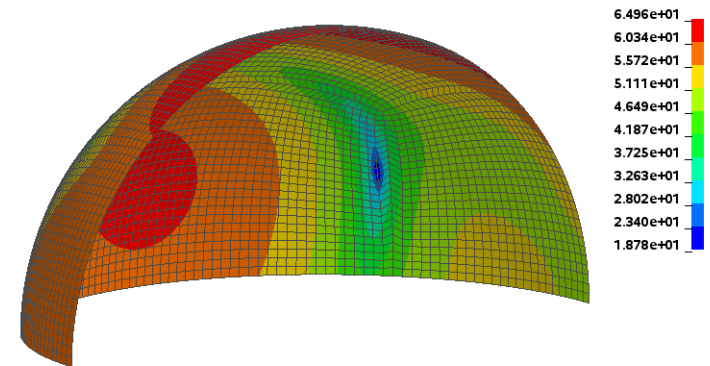
SPL distribution (dB)



An imaginary semi-sphere for better visualization of the noise distribution

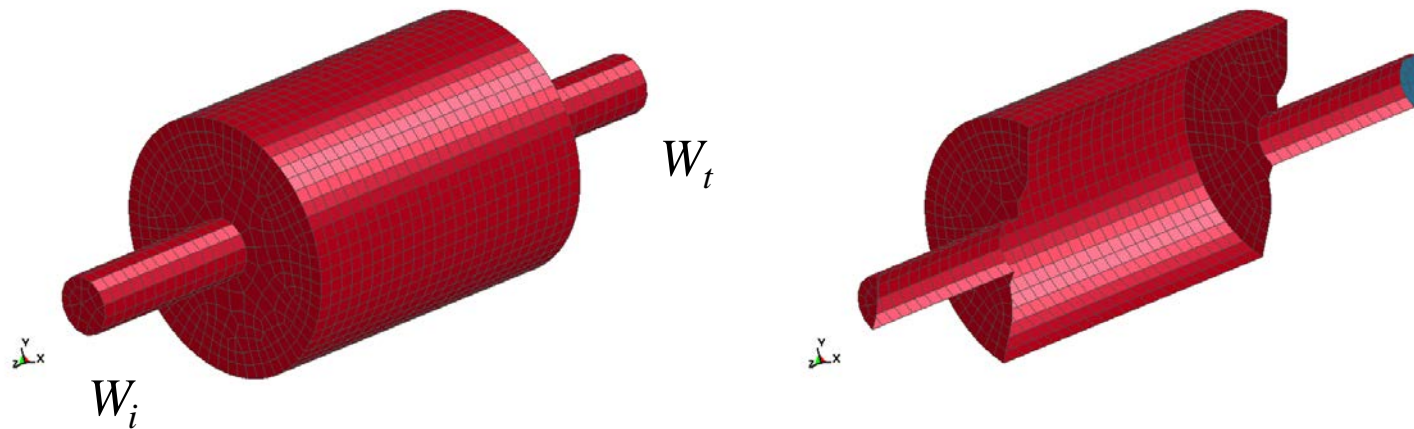


Freq = 11 Hz



Freq = 101 Hz

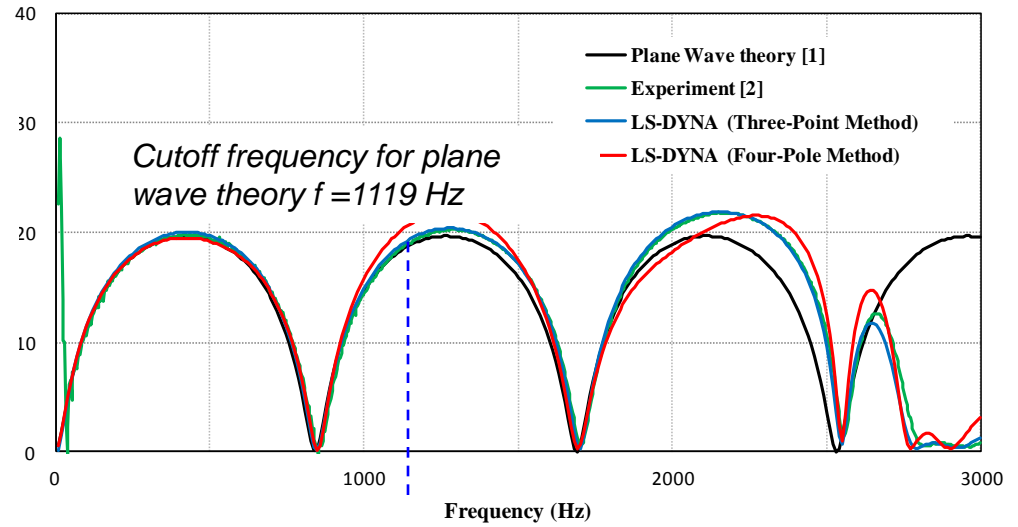
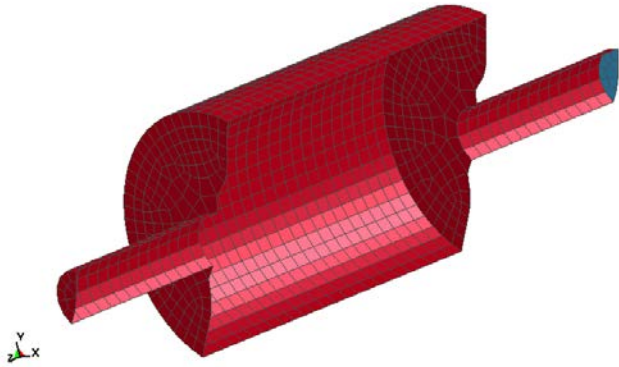
Muffler transmission loss analysis



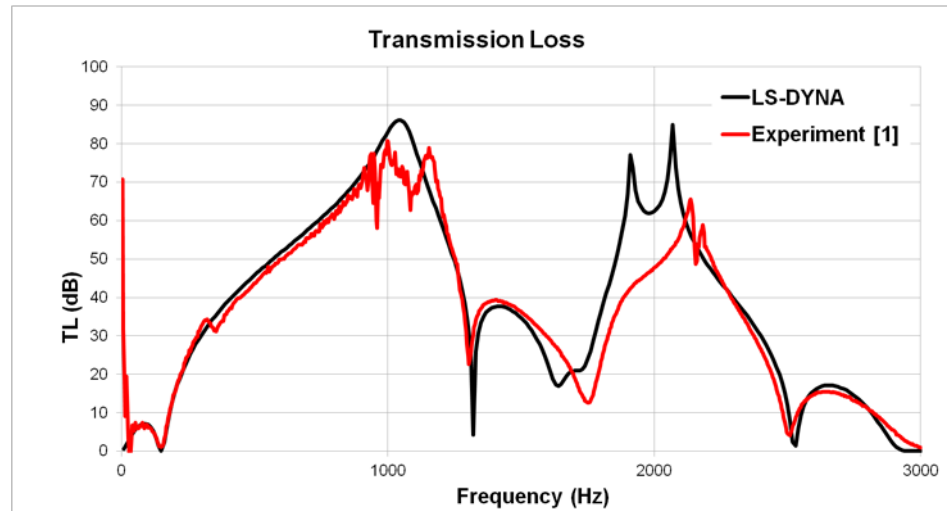
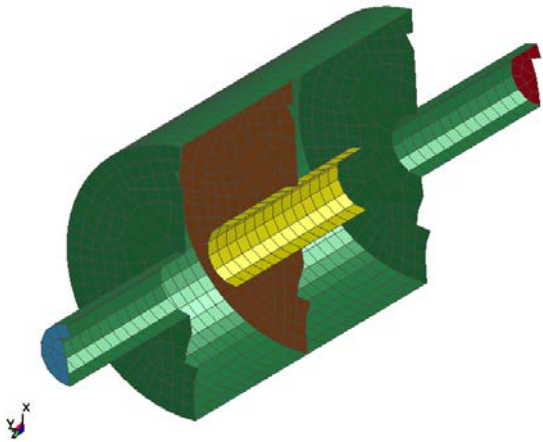
TL (Transmission loss) is the difference in the sound power level between the incident wave entering and the transmitted wave exiting the muffler when the muffler termination is anechoic (no reflection of sound).

$$TL = 10 \log_{10} \frac{W_i}{W_t}$$

Simple expansion chamber



Double expansion chamber

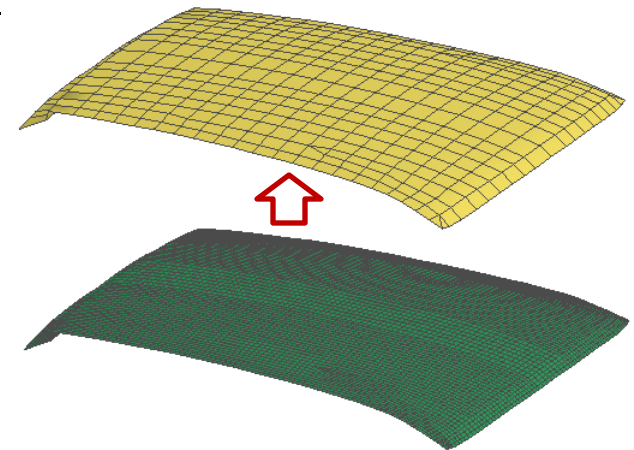


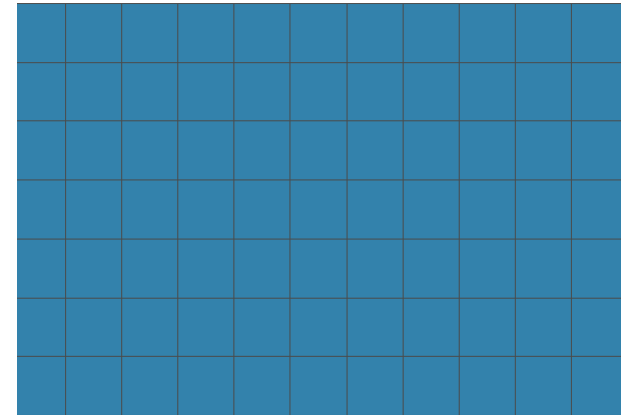
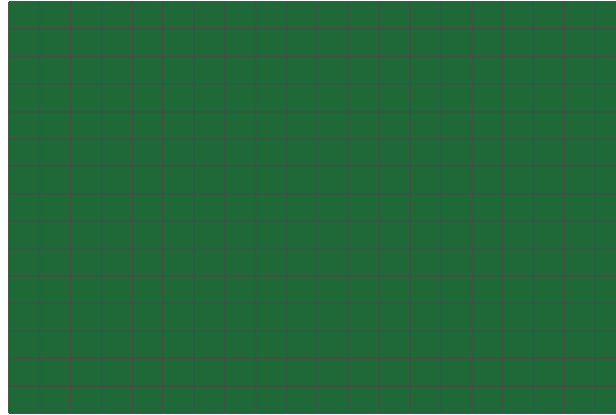
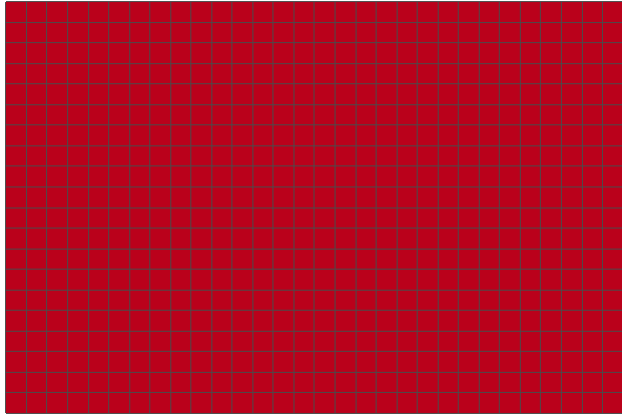
*BOUNDARY_ACOUSTIC_MAPPING

Purpose: Define a set of elements or segments on structure for mapping structural nodal velocity to boundary of acoustic volume.

Card	1	2	3	4	5	6	7	8
Variable	SSID	STYP						
Type	I	I						
Default	none	0						

<u>VARIABLE</u>	<u>DESCRIPTION</u>
SSID	Set or part ID
STYP	Set type: EQ.0: part set ID, see *SET_PART, EQ.1: part ID, see *PART, EQ.2: segment set ID, see *SET_SEGMENT.





Mesh A: 20×30 (600)

Mesh B: 15×20 (300)

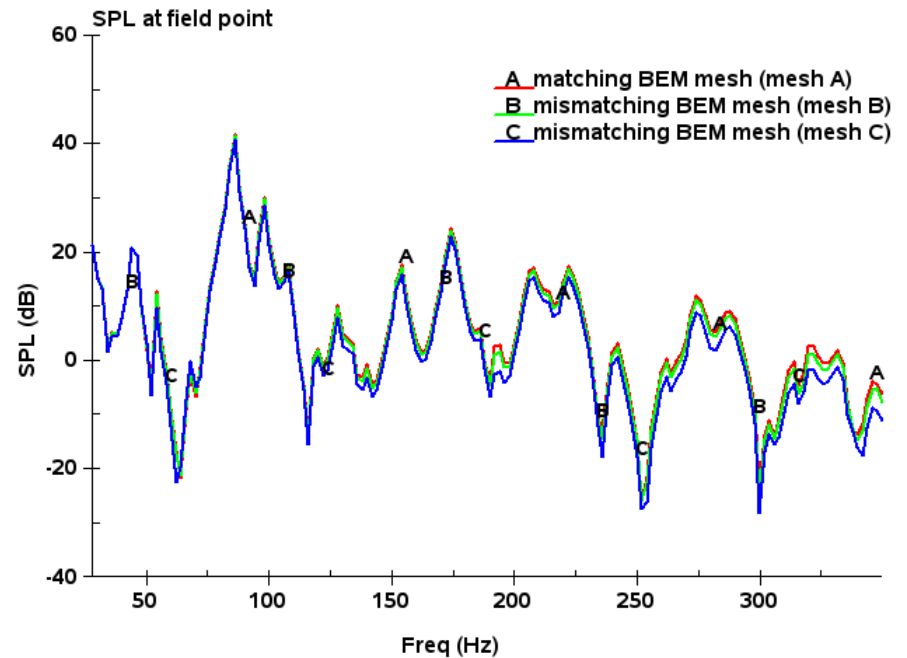
Mesh C: 7×11 (77)



Original mesh for structure surface

CPU time (Intel Xeon 1.6 GHz)

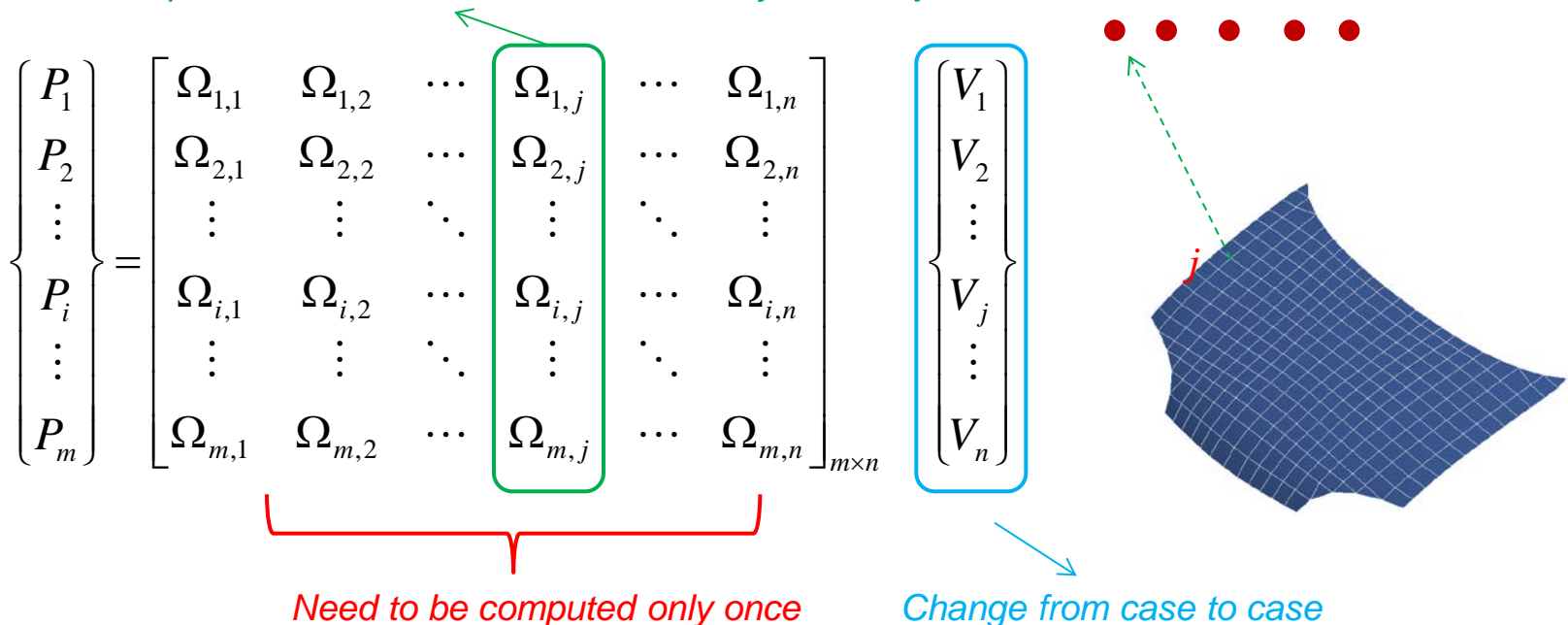
Mesh A	16 min 34 sec
Mesh B	10 min 10 sec
Mesh C	6 min 49 sec



*FREQUENCY_DOMAIN_ACOUSTIC_BEM_ATV

- It calculates acoustic pressure (and sound pressure level) at field points due to unit normal velocity of each surface node.
- ATV is dependent on structure model, properties of acoustic fluid as well as location of field points.
- ATV is useful if the same structure needs to be studied under multiple load cases.

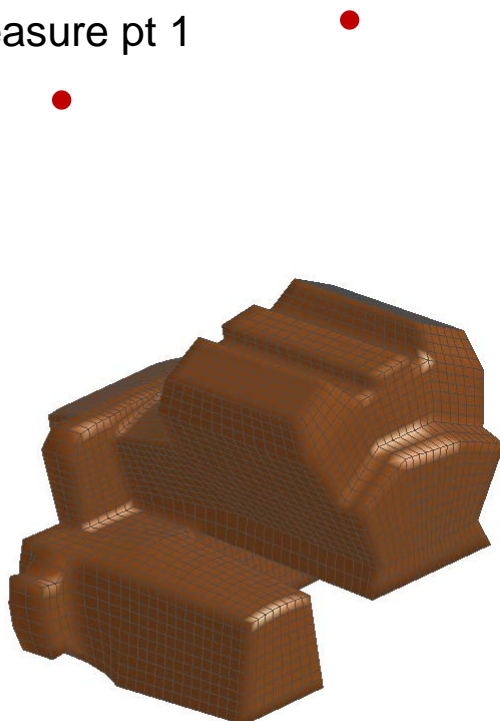
ATV at field points 1-m, due to unit normal velocity at node j



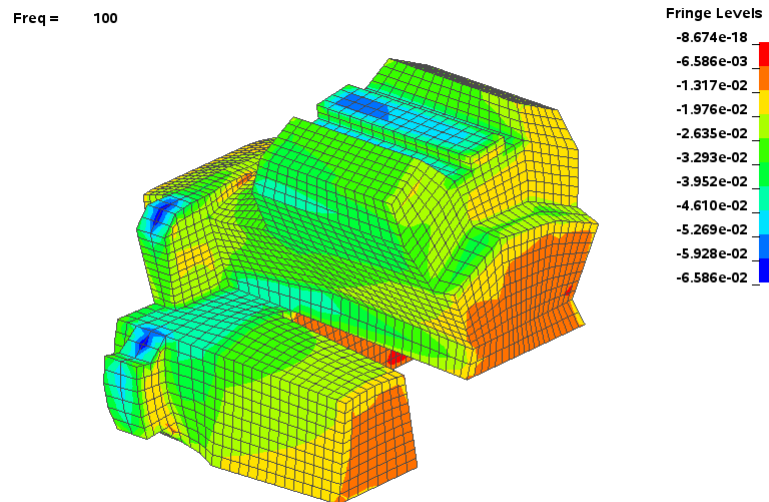
ATV of auto engine model

Measure pt 2

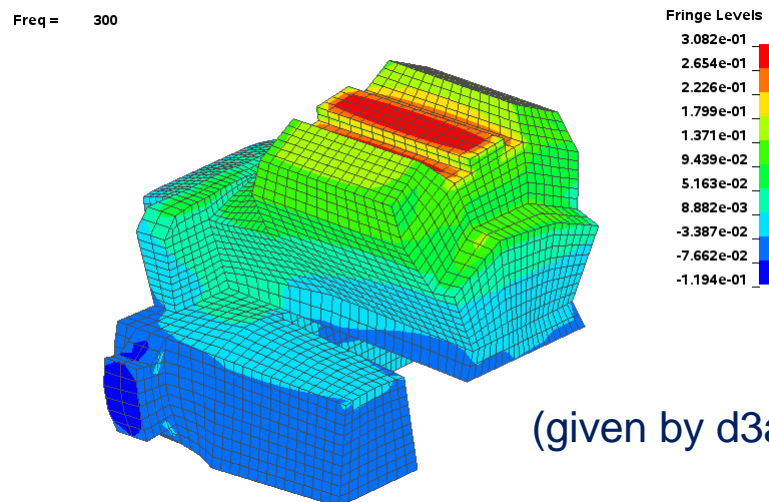
Measure pt 1



Real part of pressure ATV at pt 1



Imaginary part of pressure ATV at pt 2



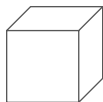
(given by d3atv)

Introduction: FEM Acoustics

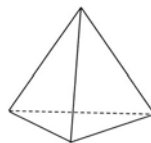
*FREQUENCY_DOMAIN_ACOUSTIC_FEM

- An alternative method for acoustics. It helps predict and improve sound and noise performance of various systems. The FEM simulates the entire propagation volume -- being air or water.
- Compute acoustic pressure and SPL (sound pressure level)
- Output binary database: `d3acs` (accessible by LS-PREPOST)
- Output ASCII database: `Press_Pa` and `Press_dB` as xyplot files
- Output frequency range dependent on mesh size
- Very fast since
 - ✓ One unknown per node
 - ✓ The majority of the matrix is unchanged for all frequencies
 - ✓ Using a fast sparse matrix iterative solver

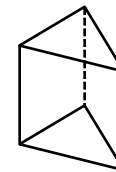
Hexahedron



Tetrahedron



Pentahedron

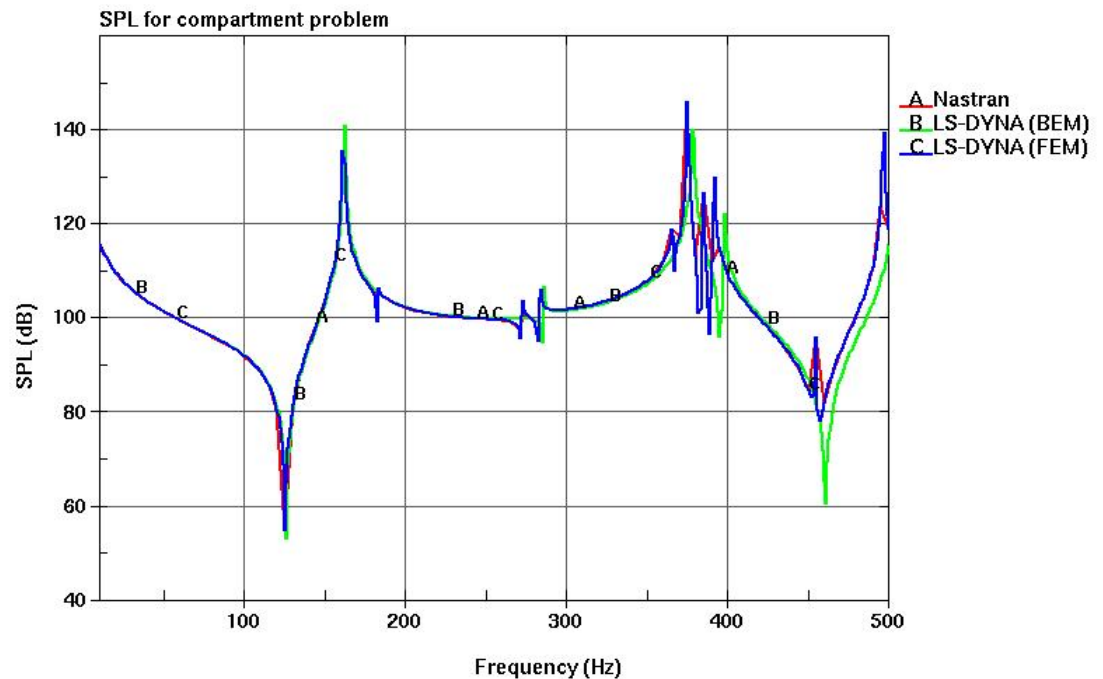
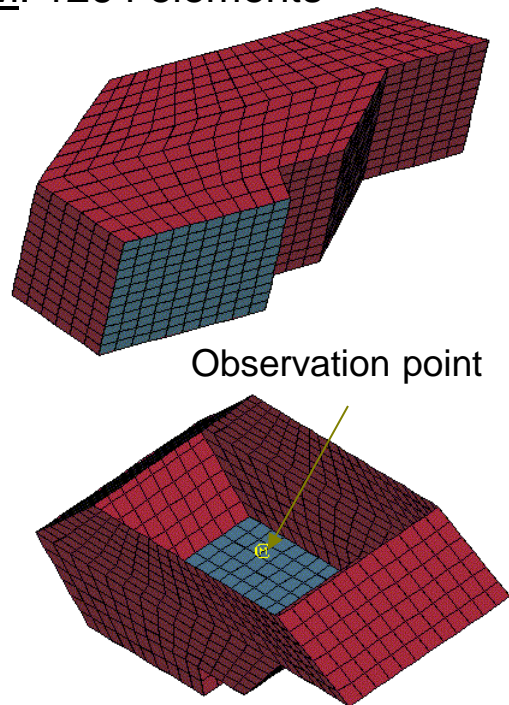


Example: compartment of vehicle

Model information

FEM: 2688 elements

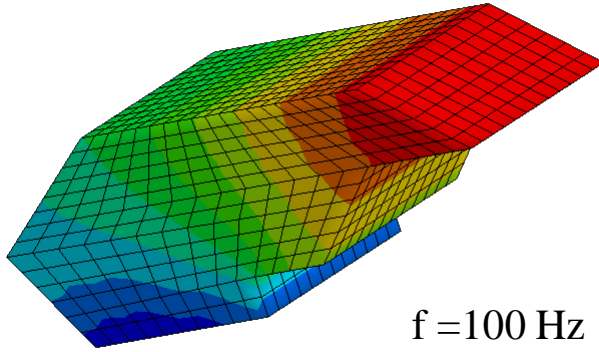
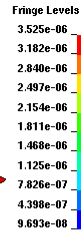
BEM: 1264 elements



Excitation of the compartment ($1.4 \times 0.5 \times 0.6$)
 m^3 by a velocity of 7mm/s

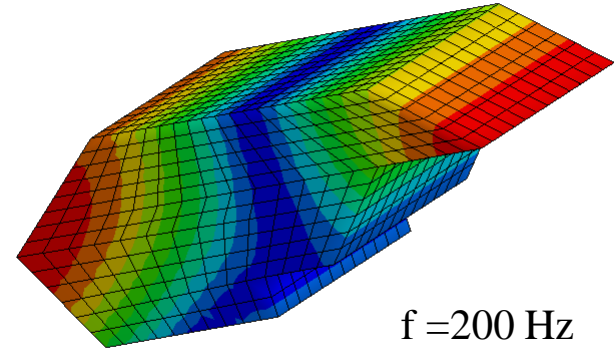
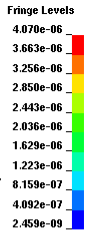
Pressure distribution

Acoustic analysis of a simplified compa
Time = 100
Contours of Z-velocity
min=9.6926e-08, at node# 108754
max=3.5252e-06, at node# 109522



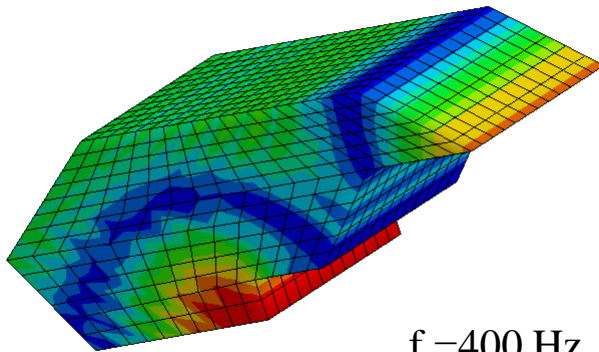
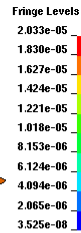
f = 100 Hz

Acoustic analysis of a simplified compa
Time = 200
Contours of Z-velocity
min=2.4588e-09, at node# 111023
max=4.0699e-06, at node# 111154



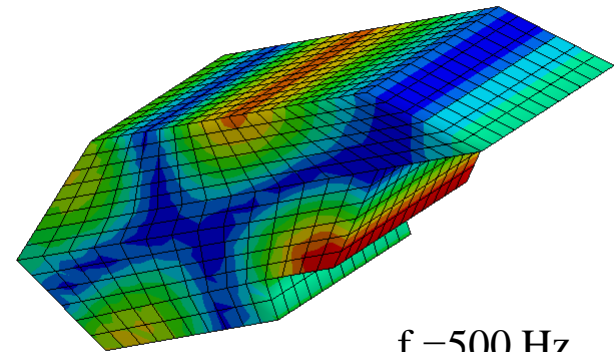
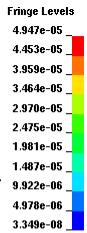
f = 200 Hz

Acoustic analysis of a simplified compa
Time = 400
Contours of Z-velocity
min=3.5245e-08, at node# 110926
max=2.0330e-05, at node# 108934



f = 400 Hz

Acoustic analysis of a simplified compa
Time = 500
Contours of Z-velocity
min=3.3494e-08, at node# 109666
max=4.9474e-05, at node# 111106



f = 500 Hz

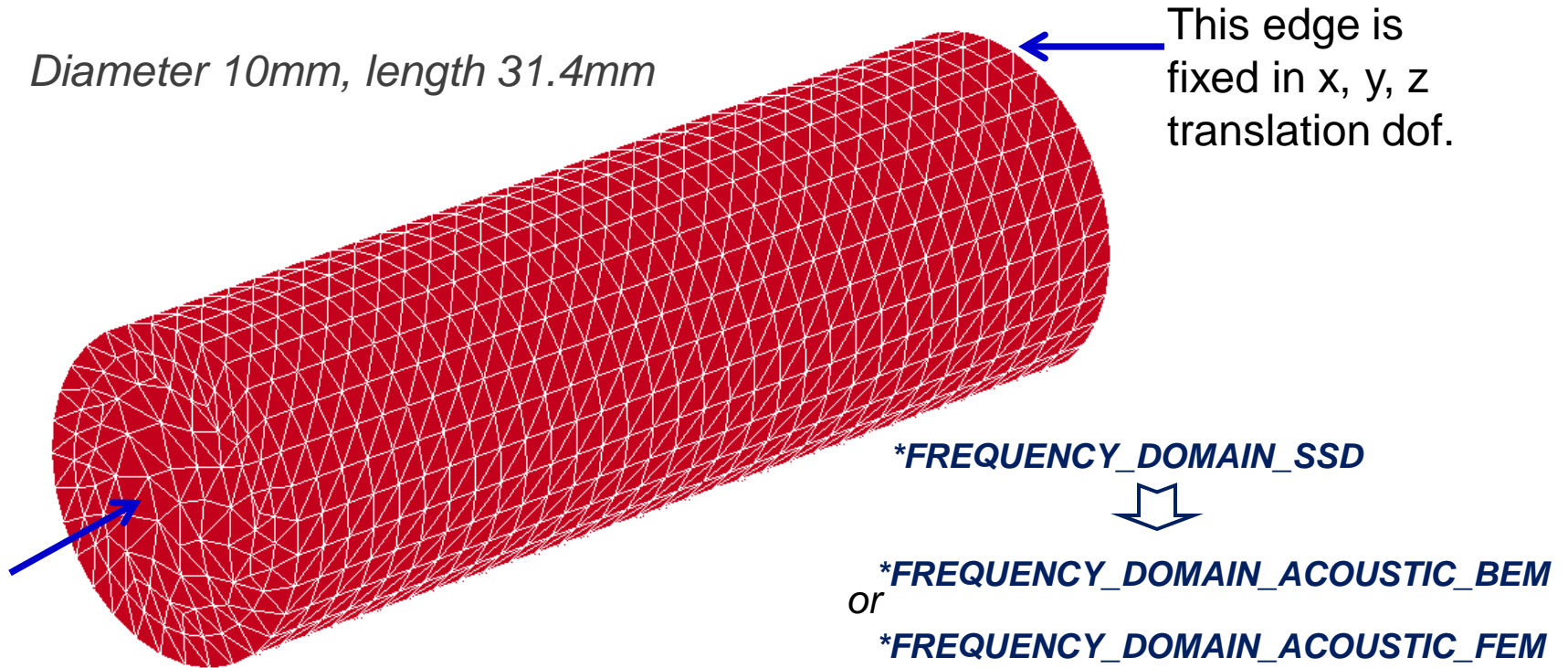
(given by d3acs)

Example: a cylinder model

Introduction

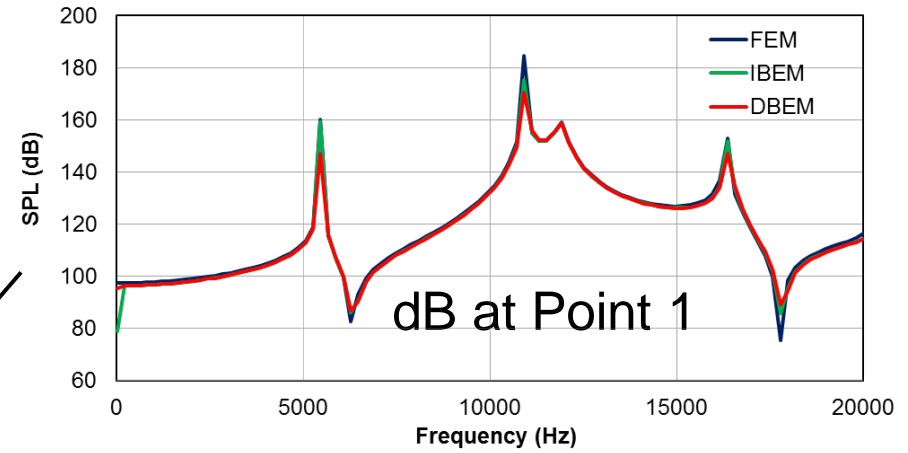
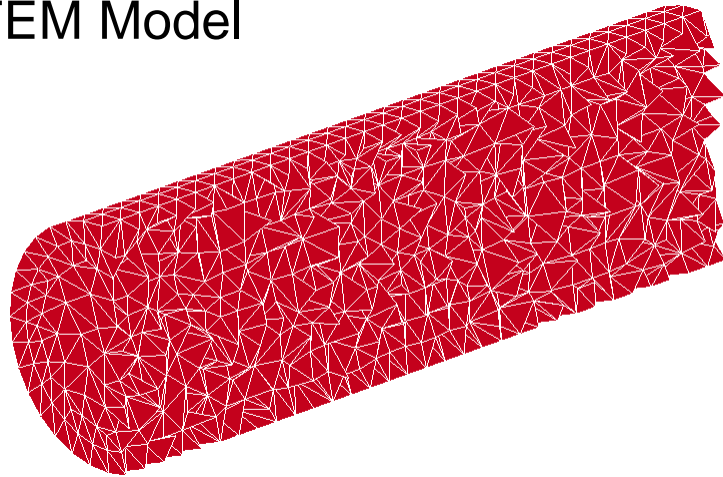
To solve an interior acoustic problem by variational indirect BEM, collocation BEM and FEM. The cylinder duct is excited by harmonic nodal force at one end.

Diameter 10mm, length 31.4mm

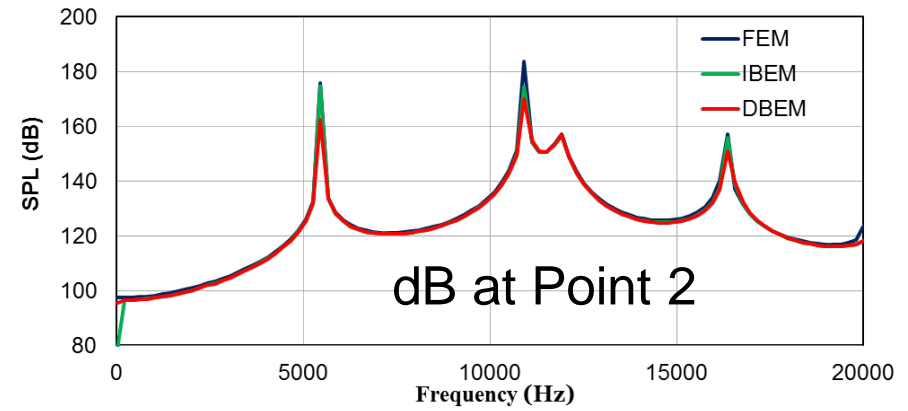
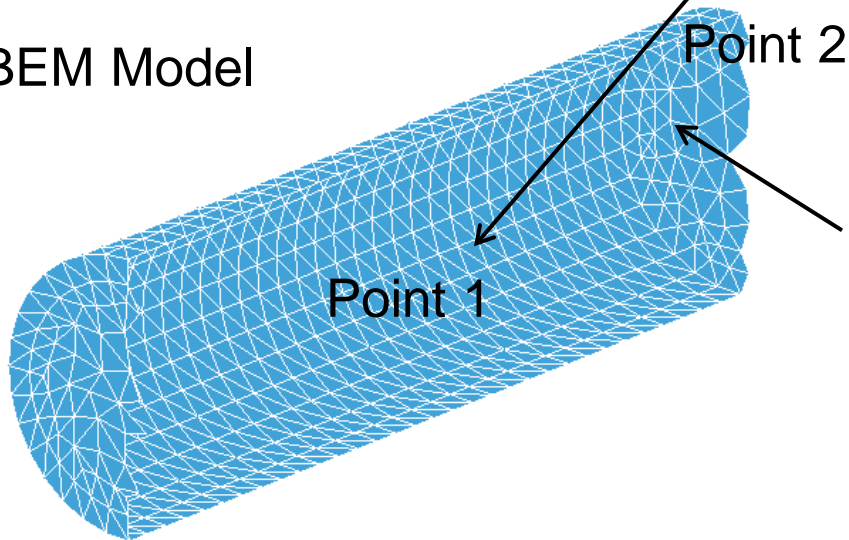


Nodal force 0.01N is applied for frequency range of 10-20000 Hz.

FEM Model



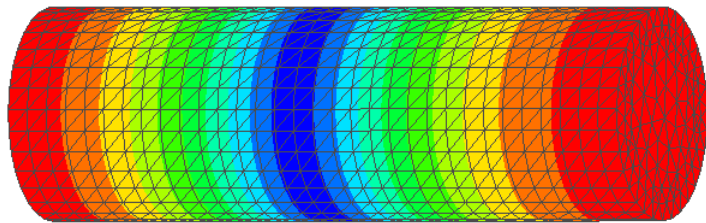
BEM Model



Acoustic pressure distribution

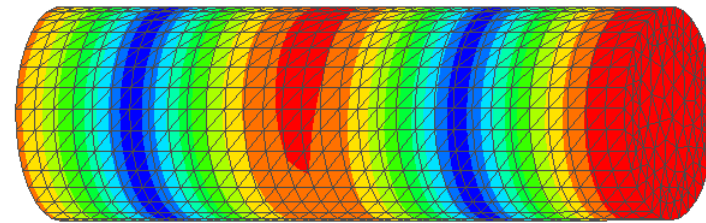
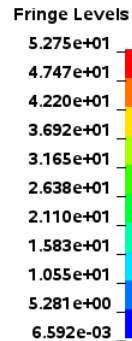
(given by d3acs)

FEM acoustic analysis following SSD ana
Time = 5000
Contours of Z-velocity
min=0.00659163, at node# 108
max=52.7459, at node# 1183

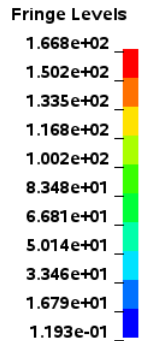


$f = 5000$ Hz

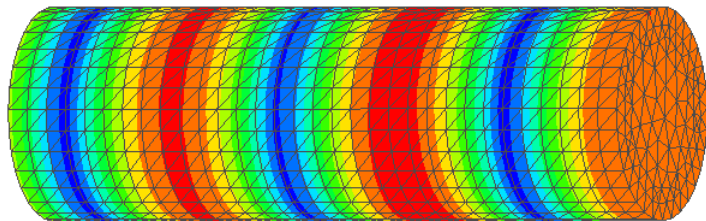
FEM acoustic analysis following SSD ana
Time = 10000
Contours of Z-velocity
min=0.119307, at node# 2538
max=166.84, at node# 1057



$f = 10000$ Hz

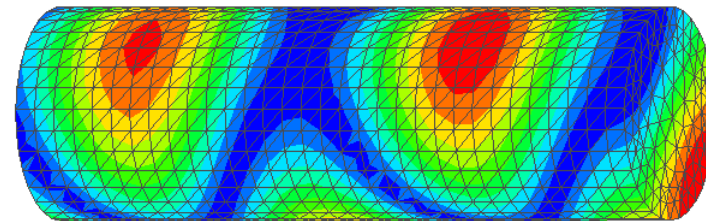
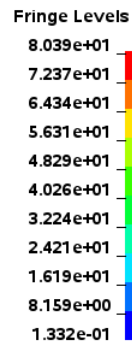


FEM acoustic analysis following SSD ana
Time = 15000
Contours of Z-velocity
min=0.133217, at node# 2845
max=80.3927, at node# 2045

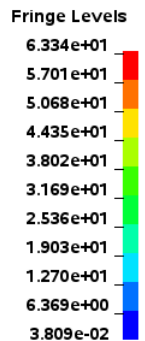


$f = 15000$ Hz

FEM acoustic analysis following SSD ana
Time = 20000
Contours of Z-velocity
min=0.0380889, at node# 2552
max=63.3429, at node# 29



$f = 20000$ Hz



7. Conclusion & future work

A set of frequency domain features have been implemented, towards NVH, durability analysis of vehicles and other vibration and acoustic analysis

- ✓ Frequency Response Function
- ✓ Steady State Dynamics
- ✓ Random Vibration & Fatigue
- ✓ Acoustic analysis by BEM/FEM
- ✓ Response spectrum analysis

Future work

- SEA method for high frequency acoustics
- Fast multi-pole BEM for acoustics
- Infinite acoustic FEM
- Fatigue analysis with strains
- **Feedbacks and suggestions from users**

Acknowledgements:

- ❖ CIMES, France
- ❖ Jaguar Landrover, UK
- ❖ JSOL, Japan
- ❖ NCAC, USA
- ❖ Parker Hannifin Corporation, USA
- ❖ Predictive Engineering, USA
- ❖ Rafael, Israel

Thank you!