

# Various aspects of composites modeling in LS-DYNA

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**Webinar: Composite Analysis**  
**26.11.2014**

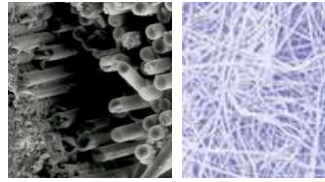
**DYNA**  
**MORE**

# Composites – a very broad term!

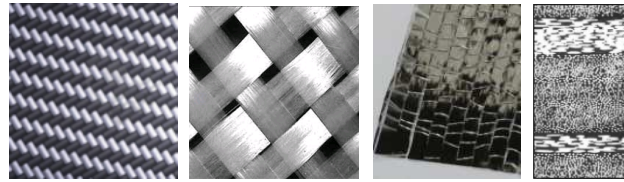
- A composite is a combination of two or more materials, differing in form or composition on a macroscale. The constituents do not dissolve or merge completely into one another, but can be physically identified and exhibit an interface.



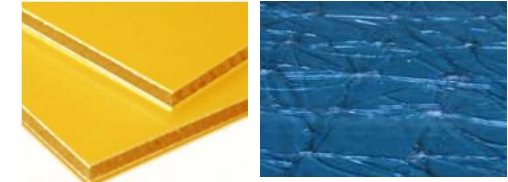
Concrete  
(cement/stone/steel)



Short/long fiber  
reinforced polymers  
(glass/PP)



Endless fiber  
reinforced polymers  
(glass/carbon/PA/PP/EP)



Sandwich/Laminates  
(alloy/polymer/..glass/PVB/...)



# Composites – classification attempts

- Based on matrix material

- Metal Matrix Composites (MMC)
- Ceramic Matrix Composites (CMC)
- Polymer Matrix Composites (PMC)

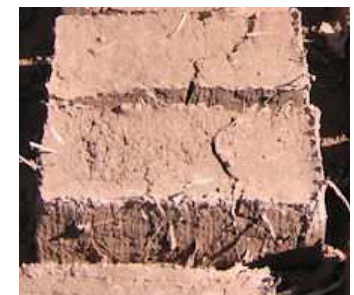
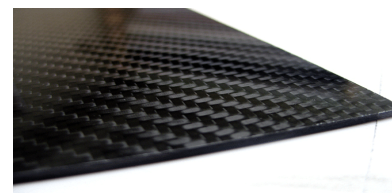
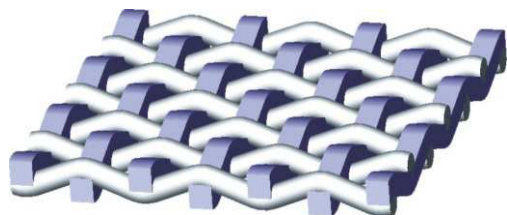


- Based on reinforcing material structure

- Particulate Composites (particles in a matrix)
- Fibrous Composites (fibers in a matrix)
- Laminated Composites (layers of various materials)
- Combination of all



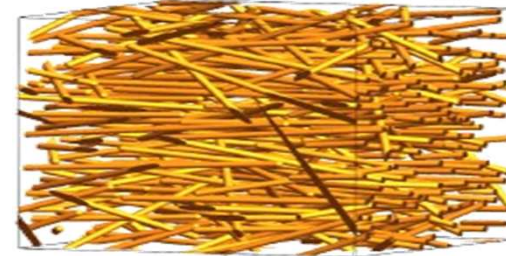
- ... and others



# Composites – What do they have in common?

- Inhomogeneous body

- non-uniform properties in the body



- Non-Isotropic behavior

- properties depend on orientation in the body

- distinguish between different levels of anisotropy

- Anisotropy: properties are different in all directions (no symmetry)

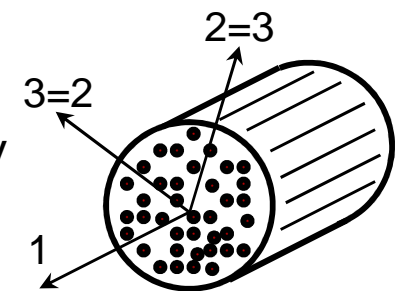
(21 unknowns)

- Orthotropy: properties are different in three perpendicular directions

(9 unknowns) (three planes of material symmetry)

- Transverse Isotropy: properties are symmetric about an axis normal to the plane of isotropy

(5 unknowns)



- Needs for FE-modeling

- appropriate material models (homogenization techniques)

- possibility to define a material coordinate system

# Agenda

- Anisotropic elastic material constants
  - rule of mixture
  - standard tests
  - remark on Poisson's Ratio
- Definition of Material-Coordinate-System
  - \*MAT\_XXX + AOPT / \*ELEMENT\_SHELL\_BETA / ...
  - mapping within the process chain
  - setup using LS-PrePost
    - S-Rail example
- General remarks
  - invariant node numbering / history variables / ...



# Anisotropic elastic material constants

- rule of mixture (i.e. lamina)

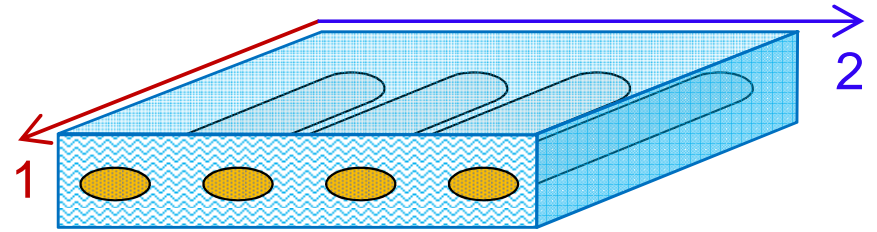
- properties of fiber and matrix

- cross-section area of fiber:  $A_f$

- cross-section area of matrix:  $A_m$

- Young's modulus, shear modulus and Poisson's ratio (fiber):  $E_f, G_f, \nu_f$

- Young's modulus, shear modulus and Poisson's ratio (matrix):  $E_m, G_m, \nu_m$



- mechanical properties of lamina

- fiber-volume and matrix-volume fraction:  $V_f, V_m$

- homogenized Young's modulus, shear modulus and Poisson's ratio:

$$E_1 = V_f E_f + V_m E_m \qquad E_2 = \frac{E_f E_m}{V_m E_f + V_f E_m}$$

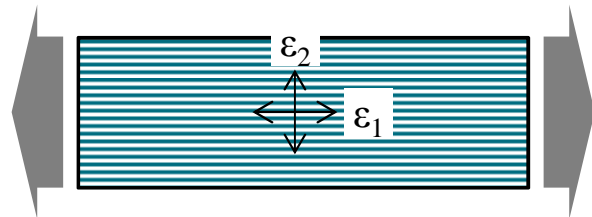
$$G_{12} = \frac{G_f G_m}{V_f G_m + V_m G_f}$$

$$\nu_{12} = V_f \nu_f + V_m \nu_m$$

# Anisotropic elastic material constants

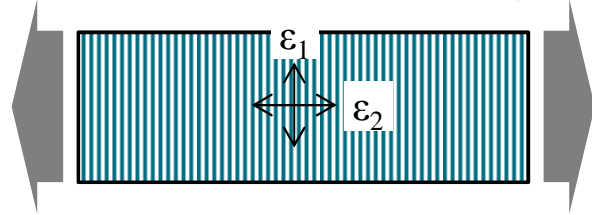
- tests with the actual composite material (the way to be preferred!)
  - necessary tests for i.e. UD-laminates

Uni-axial tensile test in 0 degree



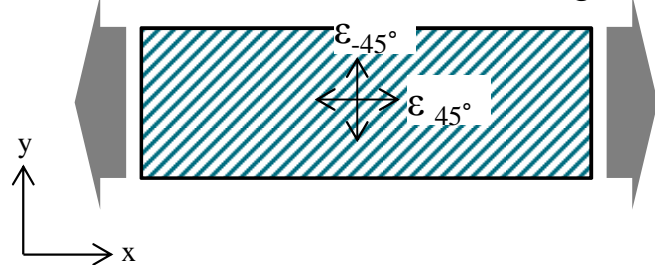
$$\sigma_1 \quad E_1 = \frac{\sigma_1}{\varepsilon_1} \quad \nu_{12} = -\frac{\varepsilon_2}{\varepsilon_1}$$

Uni-axial tensile test in 90 degree



$$\sigma_2 \quad E_2 = \frac{\sigma_2}{\varepsilon_2} \quad \nu_{21} = -\frac{\varepsilon_1}{\varepsilon_2}$$

Uni-axial tensile test in 45 degree



$$\sigma_{x45^\circ} \quad E_{45^\circ} = \frac{\sigma_{45^\circ}}{\varepsilon_{45^\circ}} \quad \nu_{45^\circ} = -\frac{\varepsilon_{-45^\circ}}{\varepsilon_{45^\circ}}$$

$$G_{12} = \frac{1}{\frac{4}{E_{45^\circ}} - \frac{1}{E_1} - \frac{1}{E_2} + \frac{2\nu_{12}}{E_1}} \quad \text{or} \quad G_{12} = \frac{E_{45^\circ}}{2(1+\nu_{45^\circ})}$$

# Anisotropic elastic material constants

- remark on Poisson's Ratio
  - all non-isotropic material models in LS-DYNA request **PRBA** ( $\nu_{21}$ )
  - symmetry of elastic stiffness matrix yields:  $\frac{\nu_{12}}{E_1} = \frac{\nu_{21}}{E_2} \rightarrow \nu_{12} = \frac{E_1}{E_2} \nu_{21}$
  - nomenclature for indices in Poisson's Ratio is not unique
- rule of thumb for using the correct Poisson's Ratio in LS-DYNA
  - make sure  $E_1 \geq E_2$
  - the larger Poisson's ratio is called the **major Poisson's ratio**
  - the smaller one is called the **minor Poisson's ratio**
- set **PRBA = minor Poisson's ratio**



# Definition of Material-Coordinate-System

- possibilities in LS-DYNA
  - \*MAT\_XXX card and AOPT>0
    - all non-isotropic material models allow to specify the definition of a globally oriented material coordinate system
    - this possibility is mainly used in sheet metal forming to initialize the anisotropy in rolling direction
  - \*ELEMENT\_T/SHELL\_BETA (shells and tshells)
    - allows the definition of a locally changing material coordinate system
  - \*ELEMENT\_SOLID\_ORTHO (solids)
    - allows the definition of a locally changing material coordinate system
  - \*PART\_COMPOSITE(\_TSHELL) (shells and tshells)
    - allows the definition of a layered part definition, i.e. for laminated structures
  - \*ELEMENT\_T/SHELL\_COMPOSITE
    - allows the definition of a layered definition on an elemental basis

# Definition of Material-Coordinate-System

- mapping within the process chain (i.e. for short fiber reinforced plastics)
  - setting up an injection molding simulation using an appropriate simulation tool (i.e. Moldflow, Moldex3D, SolidWorks Plastic, ...)
  - map material directions, orientation tensors, elastic properties, ... (using a suitable mapping tool) onto a (re-)meshed model
    - map directly onto the integration points using (i.e. \*MAT\_157 - \*MAT\_ANISOTROPIC\_ELASTIC\_PLASTIC & \*INITIAL\_STRESS\_SHELL/SOLID)
    - Solids (NHISV =  $6a_0 + 21a_1 + 6a_2 + a_3$ )

Flag	Description	Variables	#
$a_0$	Material directions	$q_{11}, q_{12}, q_{13}, q_{31}, q_{32}, q_{33}$	6
$a_1$	Anisotropic stiffness	Cij	21
$a_2$	Anisotropic constants	F, G, H, L, M, N	6
$a_3$	Stress-strain Curve	LCSS	1

- Shells (NHISV =  $2a_0 + 21a_1 + 3a_2 + a_3$ )

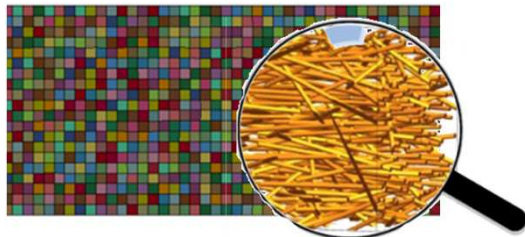
Flag	Description	Variables	#
$a_0$	Material directions	$q_1, q_2$	2
$a_1$	Anisotropic stiffness	Cij	21
$a_2$	Anisotropic constants	$r_{00}, r_{45}, r_{90}$	3
$a_3$	Stress-strain Curve	LCSS	1

# Definition of Material-Coordinate-System

- mapping within the process chain (i.e. for short fiber reinforced plastics)
  - example for shells , IHIS=3 ( $a_1 = 1$ ,  $a_0 = 1$ )  $\rightarrow$  NHISV=2+21=23
  - \*INITIAL\_STRESS\_SHELL

CARD 1	eid	nplane	nthick	nhisv	ntensor	large	nthint	nthhsv
CARD 2	t	sigxx	sigyy	sigzz	sigxy	sigyz	sigzx	eps
CARD 3	hisv1= $q_1$	hisv2= $q_2$	#3= $C_{11}$	#4= $C_{12}$	#5= $C_{13}$	#6= $C_{14}$	#7= $C_{15}$	#8= $C_{16}$
CARD 4	#9= $C_{22}$	#10= $C_{23}$	#11= $C_{24}$	#12= $C_{25}$	#13= $C_{26}$	#14= $C_{33}$	#15= $C_{34}$	#16= $C_{35}$
CARD 5	#17= $C_{36}$	#18= $C_{44}$	#19= $C_{45}$	#20= $C_{46}$	#21= $C_{55}$	#22= $C_{56}$	#23= $C_{66}$	

In material card



Drawback: inhomogeneous distribution (e.g. from previous short fiber filling simulation) in component needs individual part definition for every element

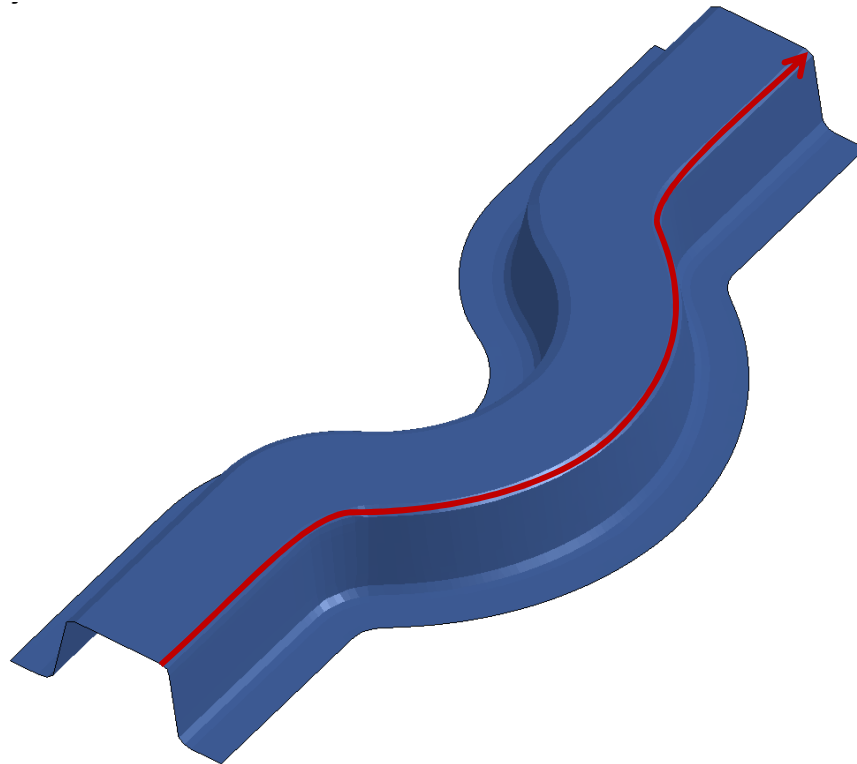
With \*INITIAL\_STRESS\_SOLID



Only one part definition for whole component. Anisotropic coefficients are part of material's history field and can therefore be initialized for each integration point individually

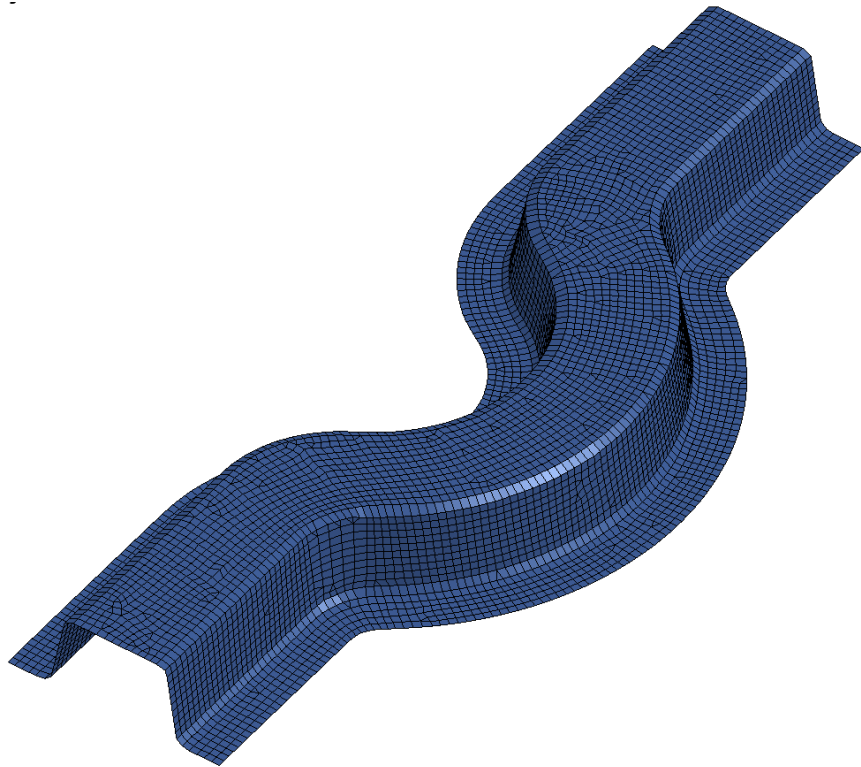
# Definition of Material-Coordinate-System

- setup using LS-PrePost – Shells
  - example using a S-Rail geometry (provided by Benteler-SGL)
  - task: define Material-Coordinate-System along the curved boundary lines

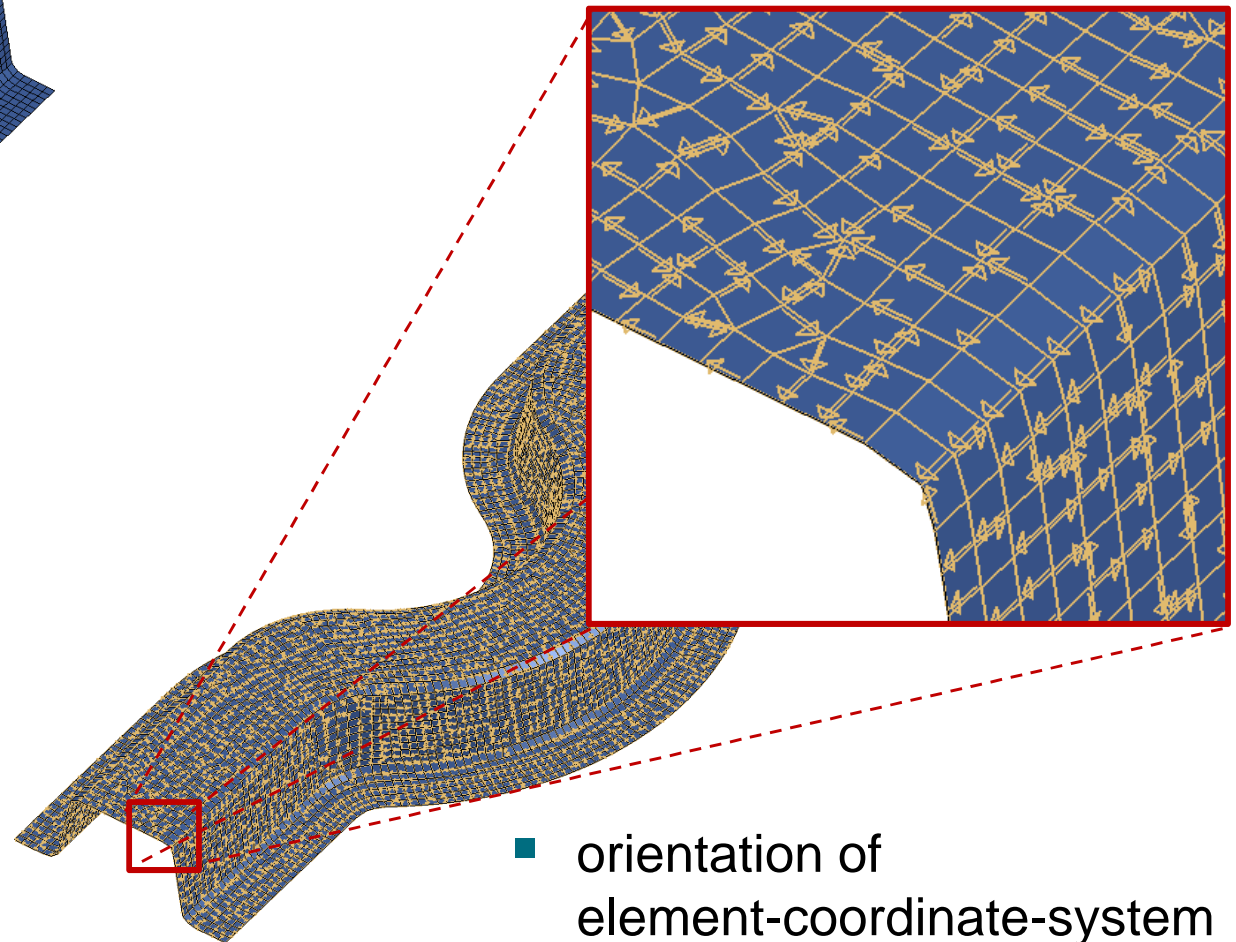


# Definition of Material-Coordinate-System

- setup using LS-PrePost – Shells
  - example using a S-Rail geometry (provided by Benteler-SGL)



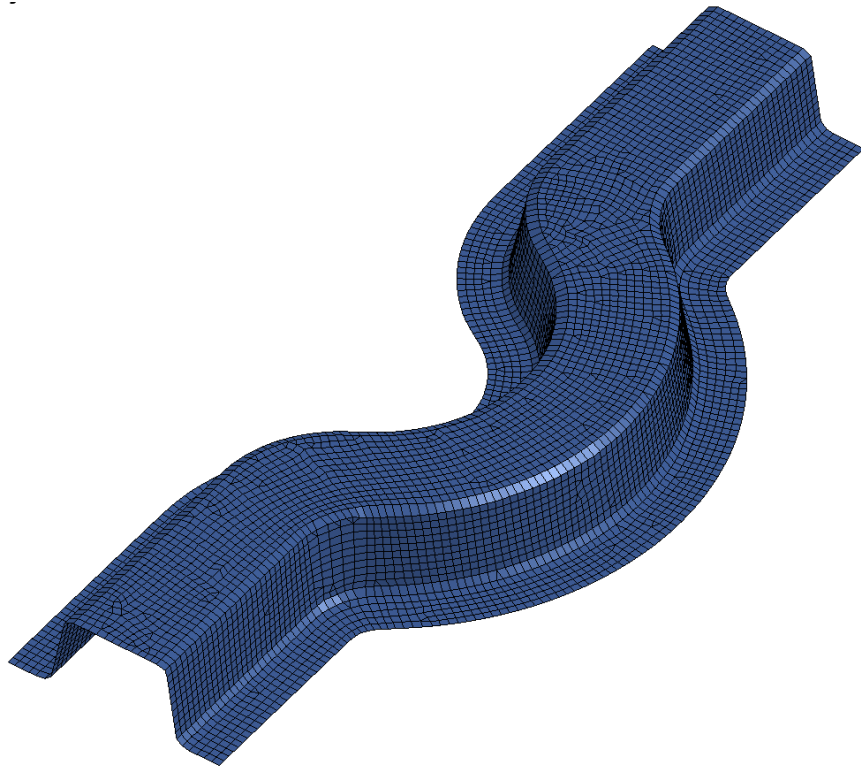
- mesh



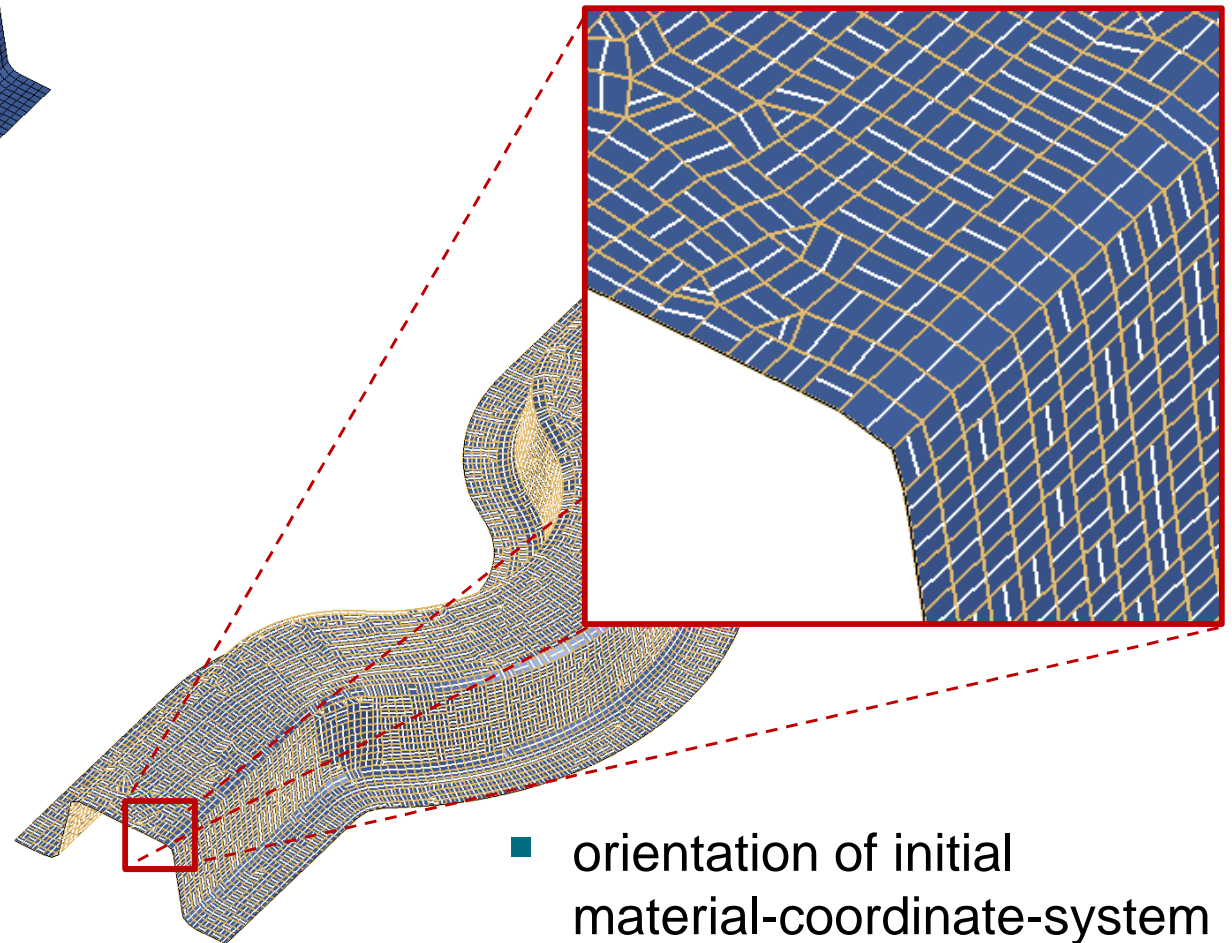
- orientation of element-coordinate-system

# Definition of Material-Coordinate-System

- setup using LS-PrePost – Shells
  - example using a S-Rail geometry (provided by Benteler-SGL)



■ mesh

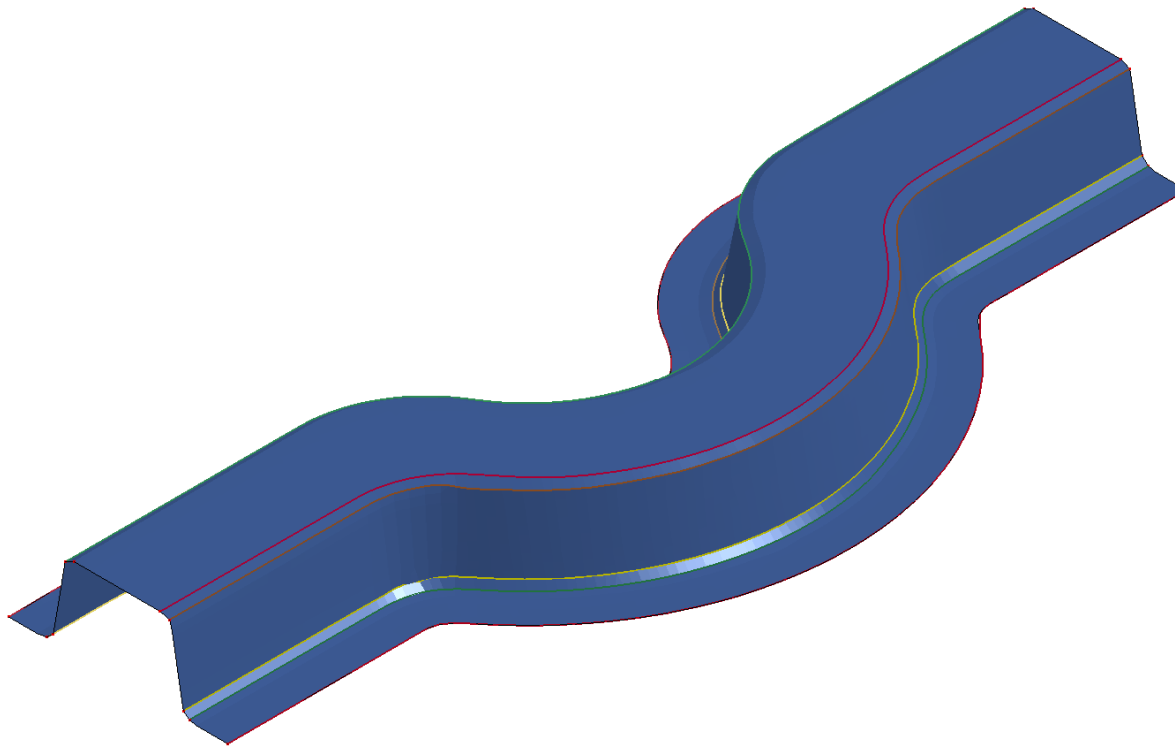


■ orientation of initial material-coordinate-system

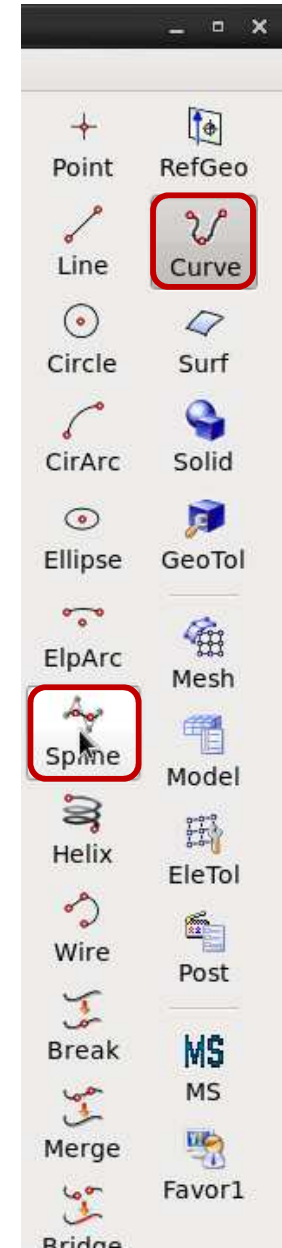


# Definition of Material-Coordinate-System

- setup using LS-PrePost – Shells
  - example using a S-Rail geometry (provided by Benteler-SGL)

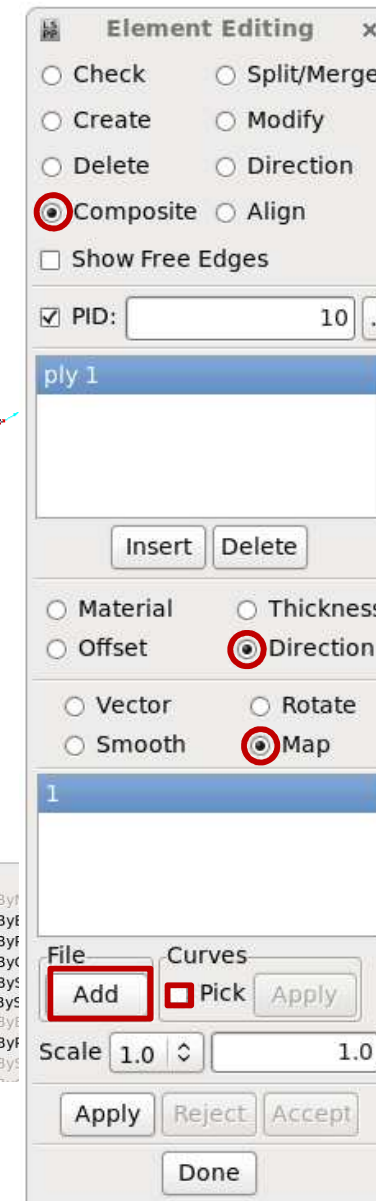
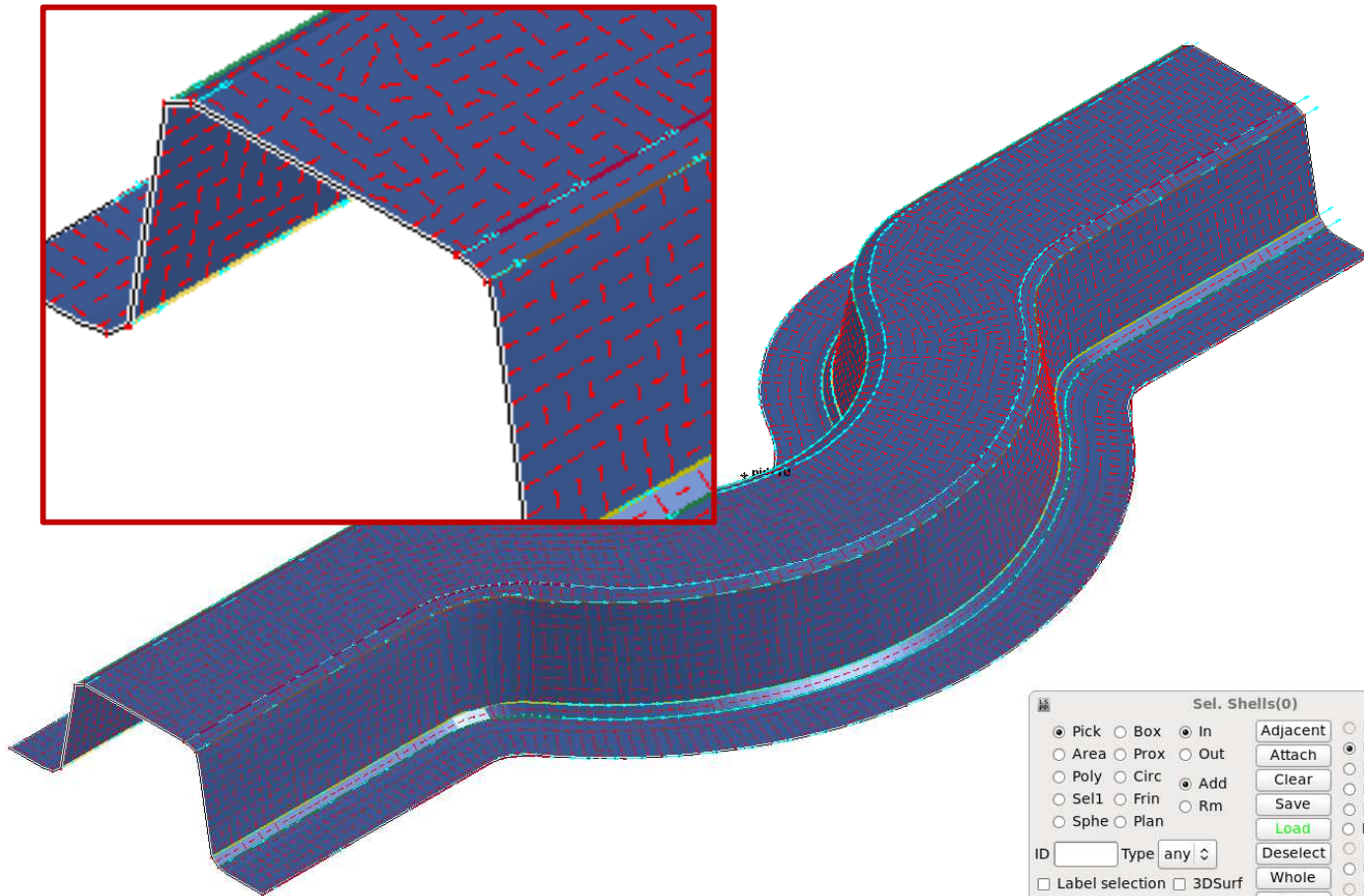


- create Spline Curves



# Definition of Material-Coordinate-System

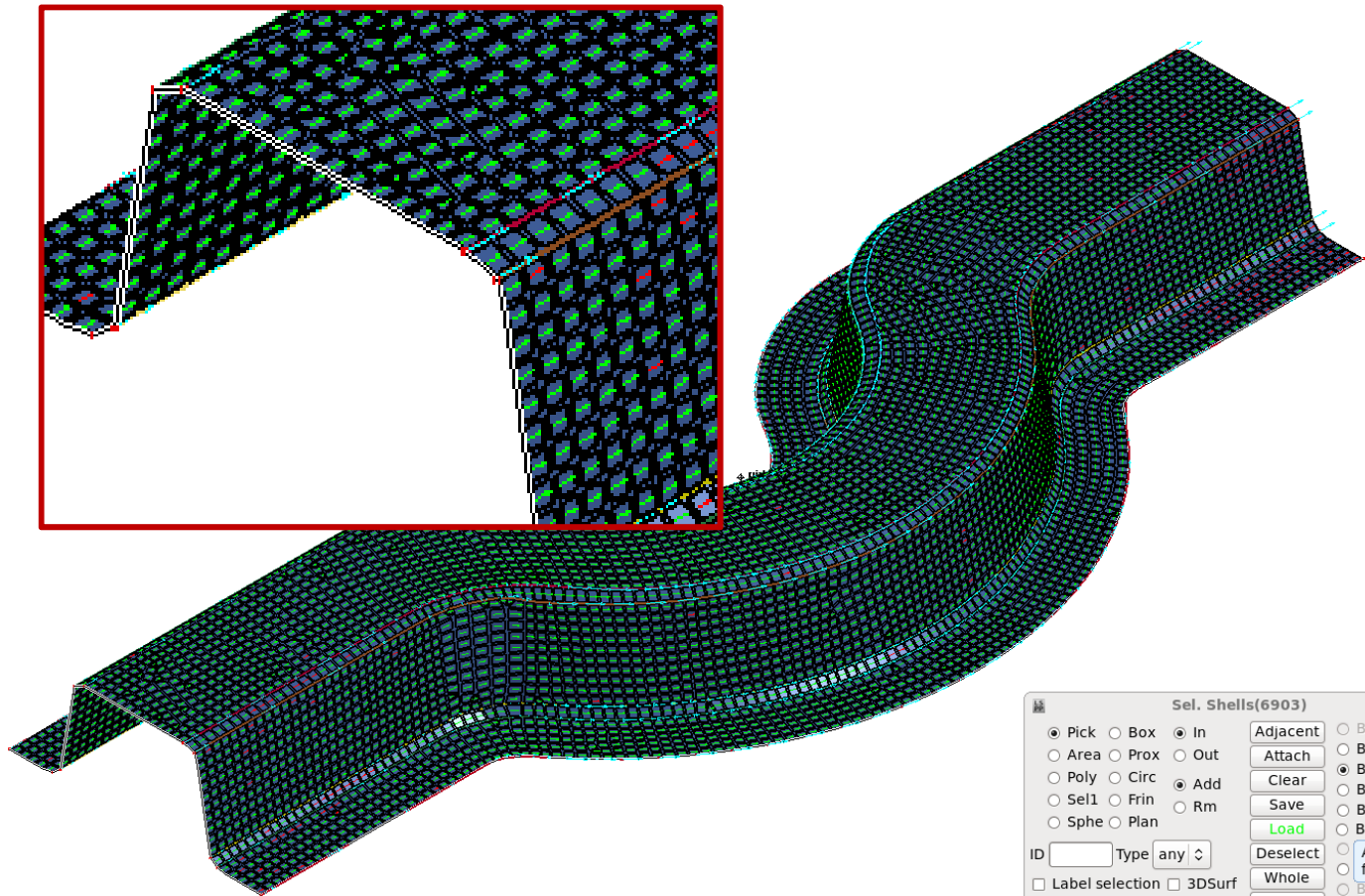
- setup using LS-PrePost – Shells



- pick spline curves and “Add”

# Definition of Material-Coordinate-System

- setup using LS-PrePost – Shells



- “Apply”

**Element Editing**

Check     Split/Merge  
 Create     Modify  
 Delete     Direction  
 Composite     Align  
 Show Free Edges

PID:

ply 1

Material     Thickness  
 Offset     Direction

Vector     Rotate  
 Smooth     Map

1

**File**    **Curves**  
  Pick

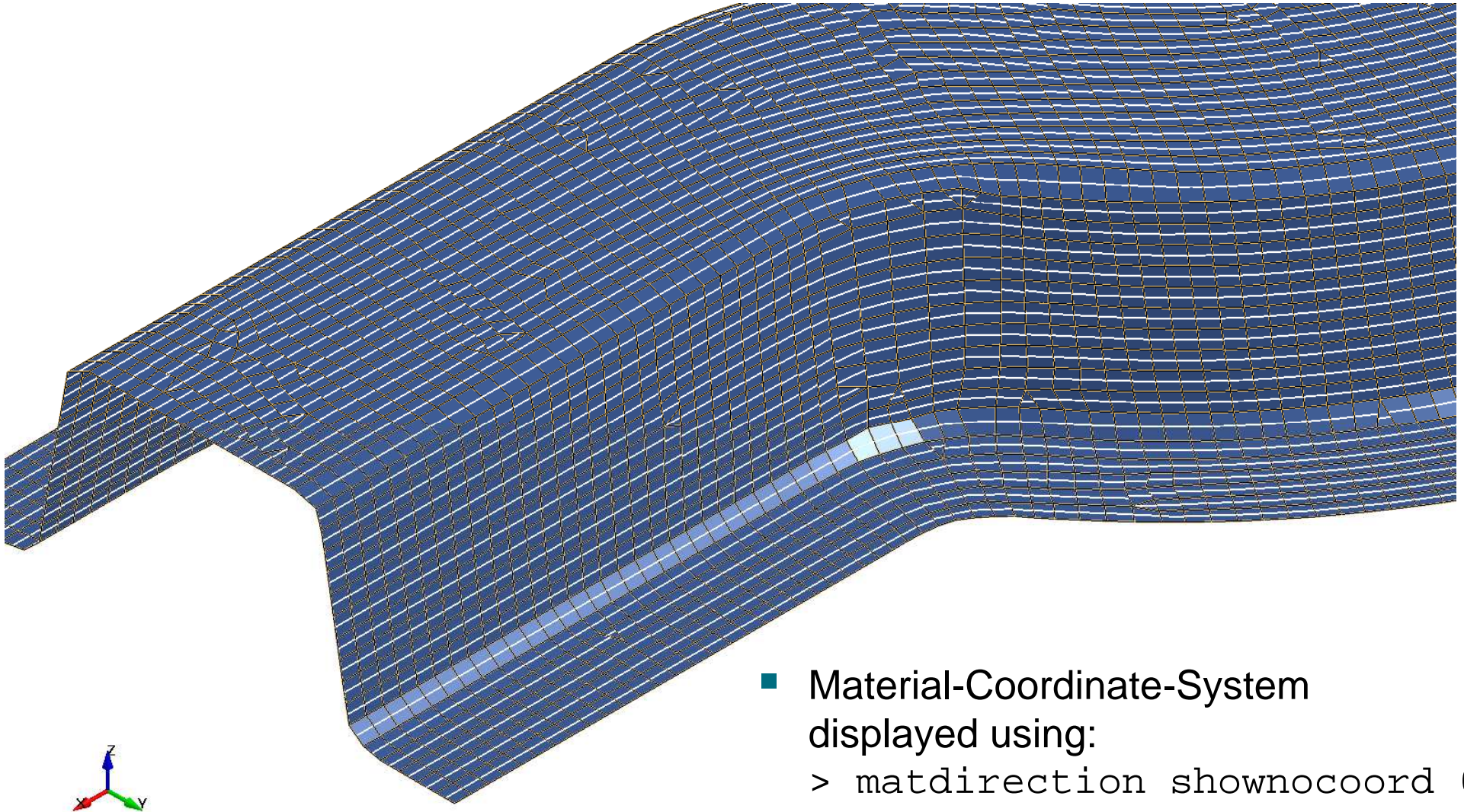
Scale

Use vector field map as direction  
plies and elements.



# Definition of Material-Coordinate-System

- setup using LS-PrePost – Shells

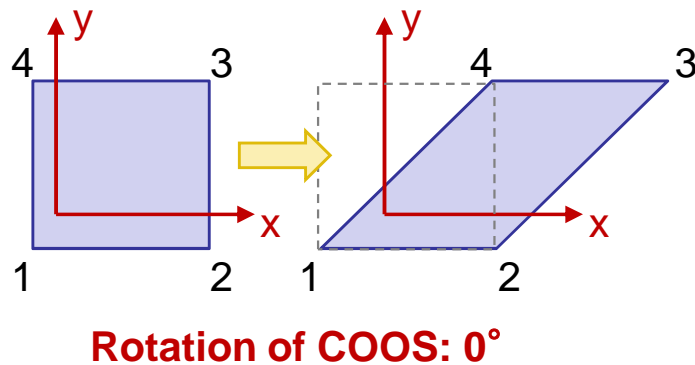


- Material-Coordinate-System displayed using:  
> `matdirection shownocoord 0`

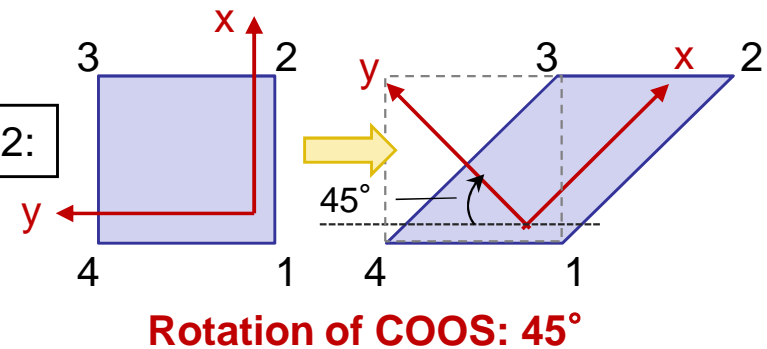
# General remarks

- we strongly recommend to use of Invariant Node Numbering
  - \*CONTROL\_ACCURACY, parameter INN
  - example: rotation of coordinate system during deformation
    - Default: without invariant node numbering

Case 1:

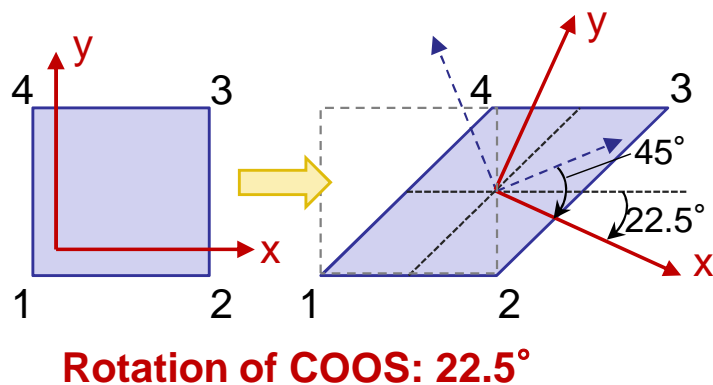


Case 2:

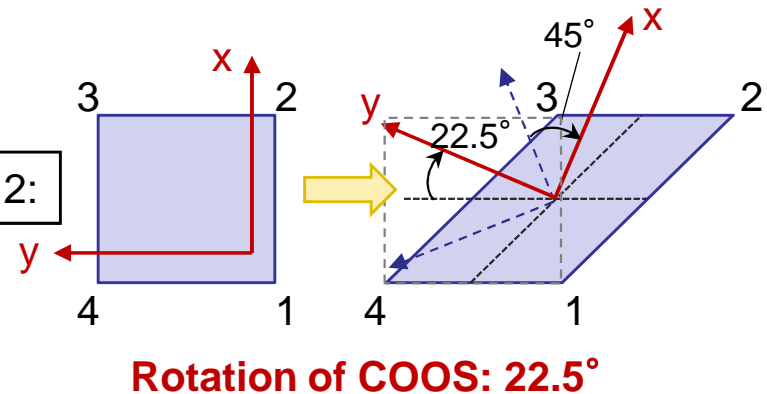


- with invariant node numbering (INN=2 in \*CONTROL\_ACCURACY)

Case 1:



Case 2:



# General remarks

- extra history variables
  - Many material models have extra history variables that help to track failure modes. A list of history variables is given here:  
<http://www.dynasupport.com/howtos/material/history-variables>
  - Set number of extra history variables to be written to d3plot with NEIPS (shells) or NEIPH (solids) in \*DATABASE\_EXTENT\_BINARY
- Output of stresses and strains in the local material coordinate system use CMPFLG=1 in \*DATABASE\_EXTENT\_BINARY

	binout	d3plot	
		global	local
CMPLFG=0	Element COOS	Global COOS	Element COOS
CMPFLG=1	Material COOS	Material COOS	Undefined



## General remarks

- For detailed post-processing request all through thickness IPs with MAXINT in \*DATABASE\_EXTENT\_BINARY
- \*DATABASE\_BINARY\_D3PART & \*DATABASE\_EXTENT\_D3PART allow to specify (detailed) output settings for selected parts
- Shell bulk viscosity may aid stability  
use \*CONTROL\_BULK\_VISCOSITY, TYPE=-1 or -2
- Adding \*DAMPING\_PART\_STIFFNESS to composite parts may decrease noise when elements start to fail
- Use NFAIL1 (under-integrated shells) and NFAIL4 (fully-integrated shells) in \*CONTROL\_SHELL to remove highly distorted elements
- New options W-MODE & STRETCH (Card 3 in \*CONTROL\_SHELL) may help to remove highly distorted elements, too

**Thank you very much for your attention!**