



Sebastian Kreissl, Thomas Senner, Arnulf Lipp, Josef Meinhardt.

# INDUSTRIAL FORMING SIMULATION OF MULTI-LAYERED UD NON-CRIMP-FABRICS.

13. LS-DYNA FORUM, 07.10.2014, BAMBERG.

**BMW  
GROUP**



# OUTLINE.

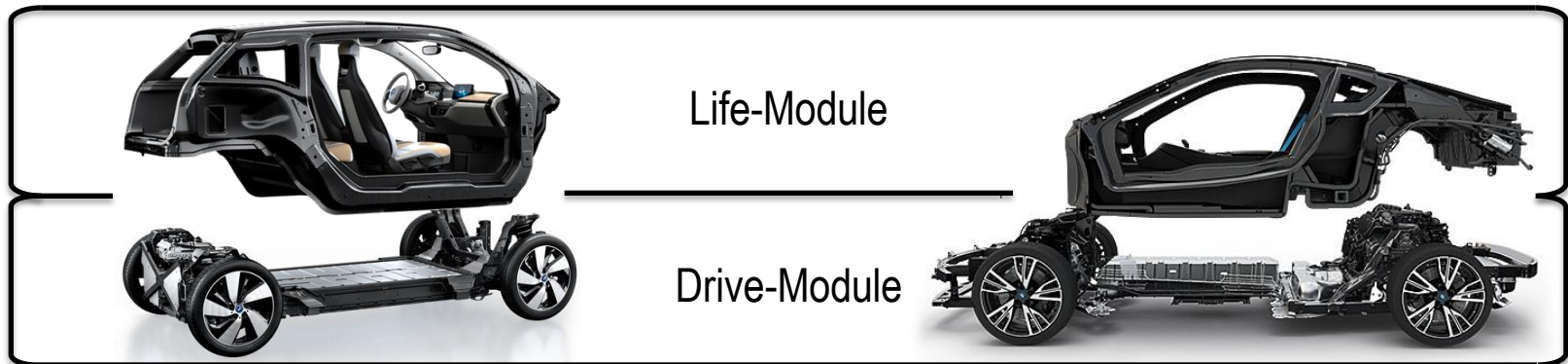
- BMW i.
- Production Process of CFRP Shell Structures.
- Large Scale Production of CFRP Parts.
- Semi-finished Carbon Fiber Products.
- Challenges for the Simulation.
- Strategy for Modelling of Unidirectional Non-Crimp-Fabrics.
- Simulation Results for Prototype Part.

# BMW i. ELECTROMOBILITY & LIGHTWEIGHT CONSTRUCTION.

BMW i3



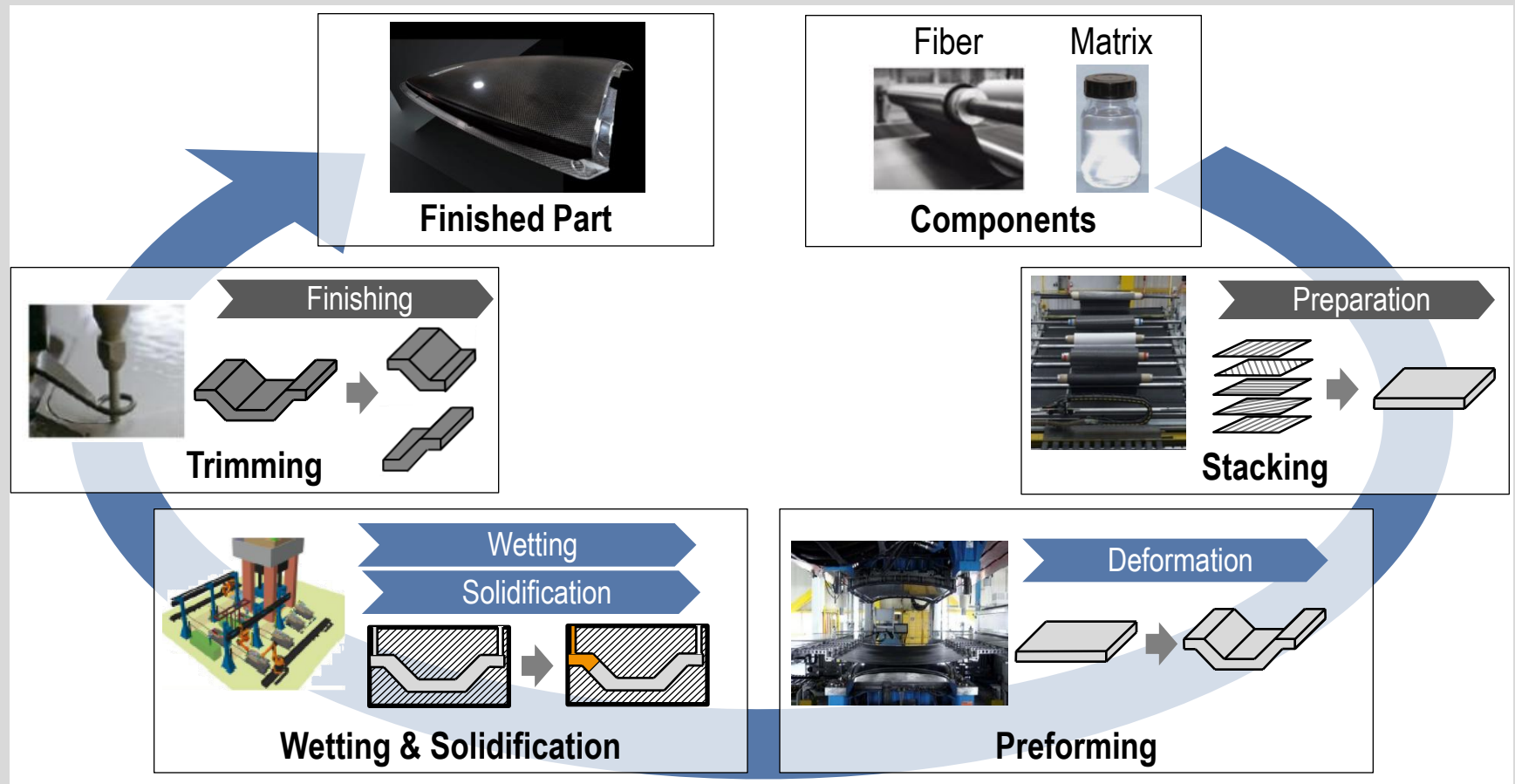
BMW i8



Life-Module

Drive-Module

# PRODUCTION PROCESS OF CFRP SHELL STRUCTURES. RESIN TRANSFER MOLDING (RTM) PROCESS.



# LARGE-SCALE PRODUCTION OF CFRP PARTS. INDUSTRIAL AUTOMATION.

## Single Item Production.

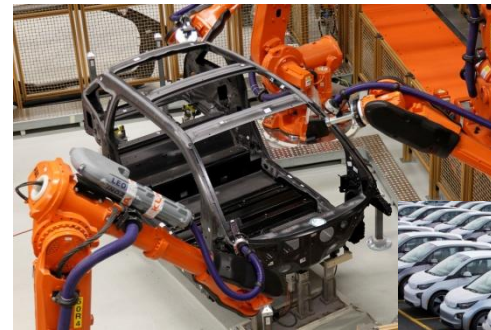


[www.boeing.com](http://www.boeing.com)



- Small number of units.
- Highly flexible.
- Long cycle/process times.

## Large-Scale Production.



- Large number of units.
- Highly automated.
- Short cycle/process times.

⇒ Forming simulation to avoid cost and time intensive changes in the tooling /process.

# SEMI-FINISHED CARBON FIBER PRODUCTS. EXAMPLES.

Fiber/Roving:

3K Roving

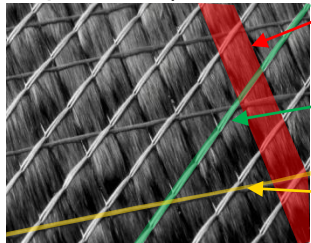


50K Roving



Textile:

Unidirectional non-crimp-fabric (UD-NCF)



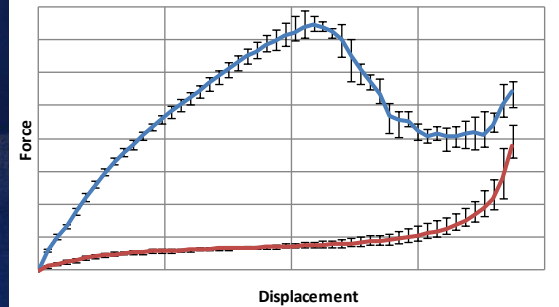
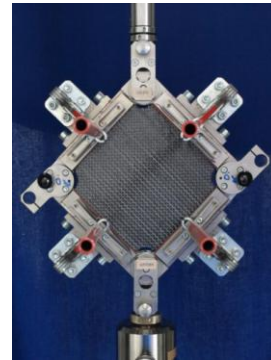
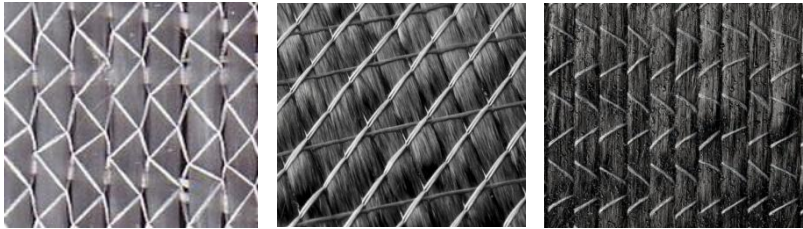
Carbon fiber roving.

Synthetic stitch thread.

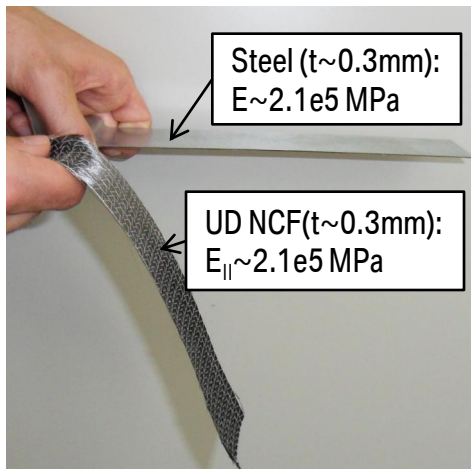
Glasfiber thread.

# CHALLENGES FOR THE SIMULATION. EXCERPT.

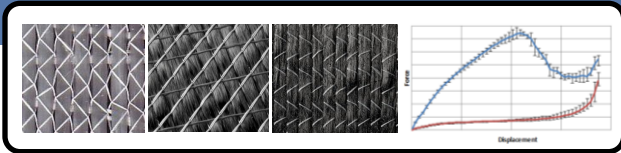
## Various Material Types.



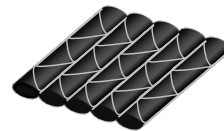
## Bending Stiffness.



# STRATEGY FOR MODELING UD-NCF. MODULAR APPROACH.

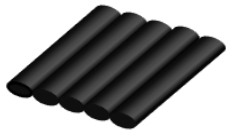


## UD-NCF



Composition of at least two structures and materials.

## Modularization and Characterization



UD fiber structure:

- Compact structure.
- Nonlinear elastic material.

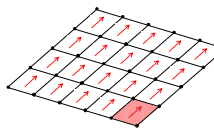
+



Warp-knitted stitch structure:

- Net-like structure.
- Nonlinear elastic material with failure.

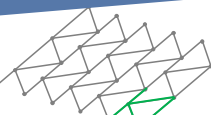
## Simplified Modeling



UD fiber model:

- Contin. approach (shell elements).
- UD fiber material model.

+

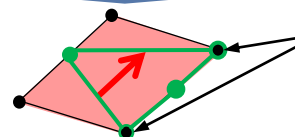


Warp-knitted stitch model:

- Discrete approach (beam elements).
- Cable material model

## Representative Unit Cell Model

Resulting macroscopic material behavior by superimposing both models.



Coincident nodes.

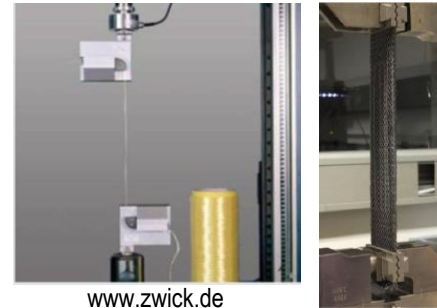
Senner et al.: A modular modeling approach for describing the in-plane forming behavior of unidirectional non-crimp-fabrics, Production Engineering Research and Development, DOI 10.1007/s11740-014-0561-z, pp 1-9



# STRATEGY FOR MODELING UD-NCF. MODULAR APPROACH.

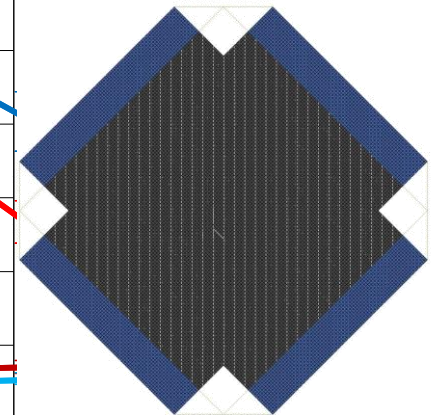
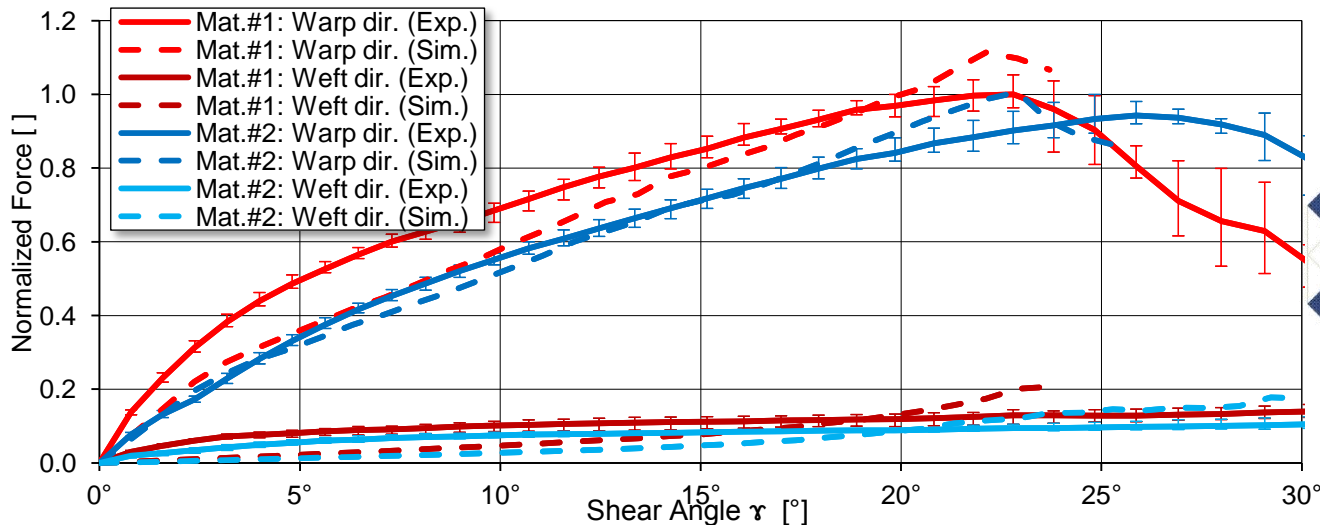
## Calibration:

- Stitching: tensile test of stitch thread.
- UD-NCF: tensile test ( $\perp$  to fibers).



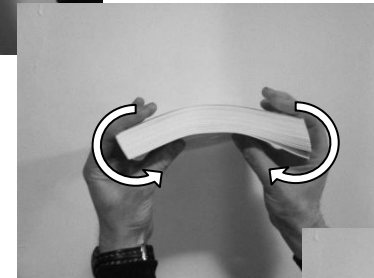
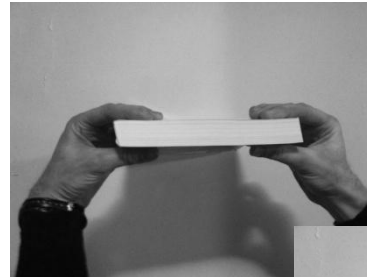
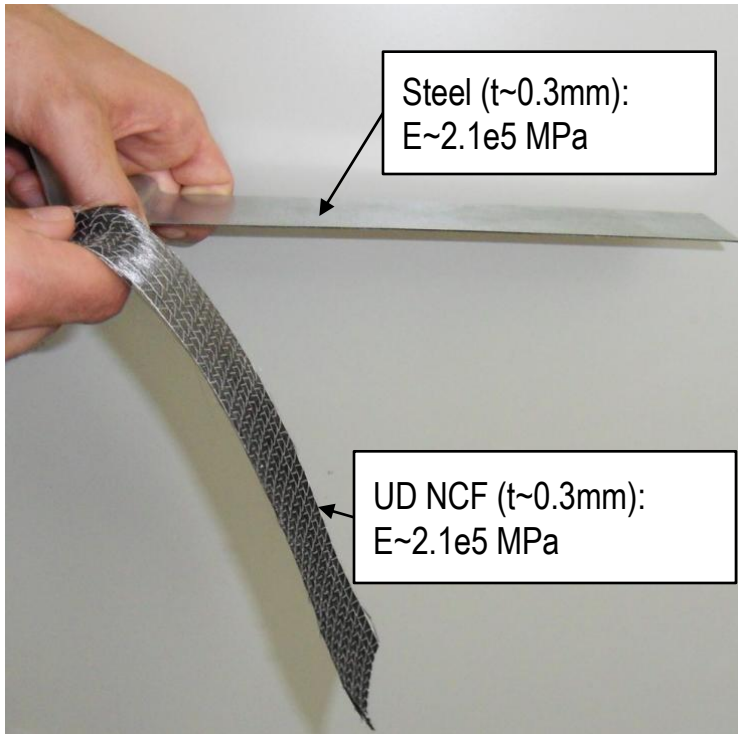
## Validation:

### Picture-Frame Test.



Senner et al.: A modular modeling approach for describing the in-plane forming behavior of unidirectional non-crimp-fabrics, Production Engineering Research and Development, DOI 10.1007/s11740-014-0561-z, pp 1-9

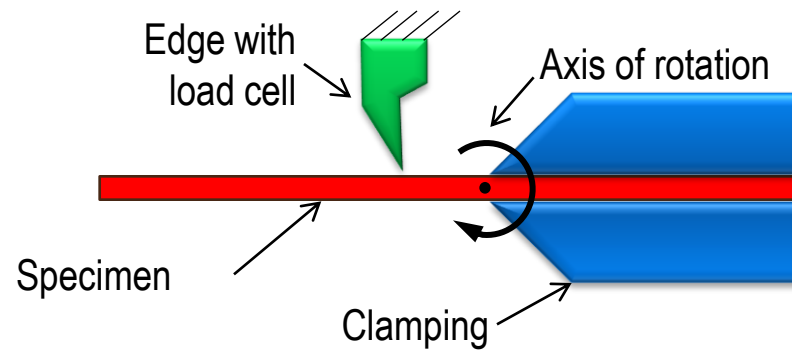
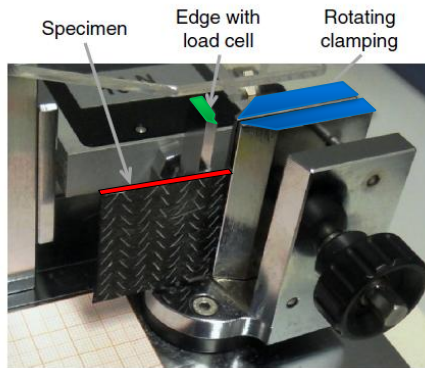
# STRATEGY FOR MODELING UD-NCF. BENDING STIFFNESS.



Discontinuity:  
low bending stiffness  
due to sliding of fibers.

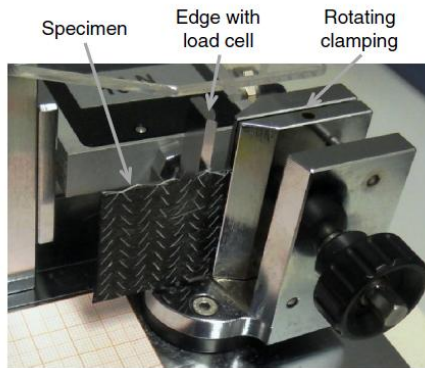
[www.xcracer.com](http://www.xcracer.com)

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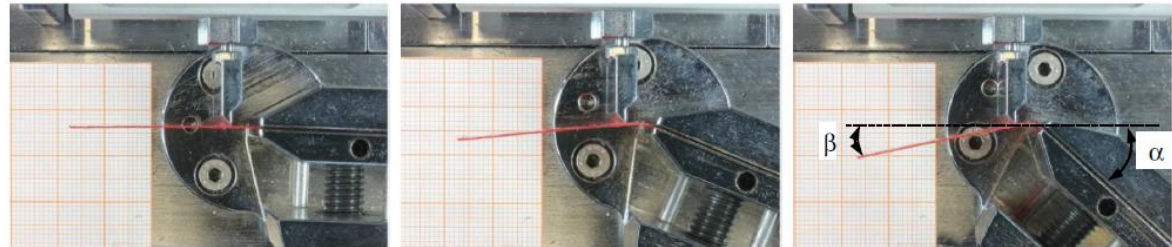


T. Senner et al.: Bending of unidirectional non-crimp-fabrics: experimental characterization, constitutive modeling and application in finite element simulation, Production Engineering Research and Development, DOI 10.1007/s11740-014-0568-5, pp 1-10.

# STRATEGY FOR MODELING UD-NCF. BENDING STIFFNESS.



## Continuous material (Polypropylene)

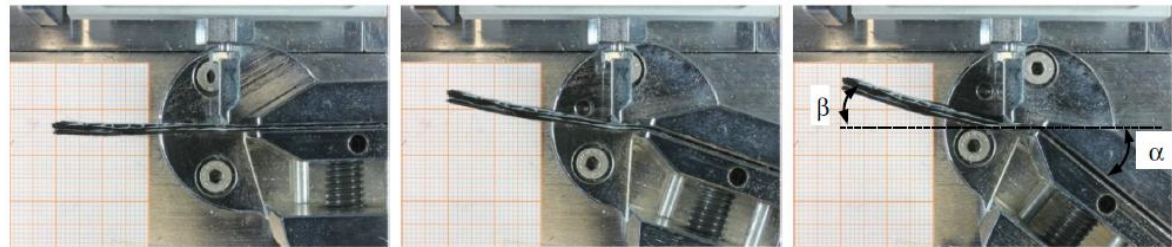


$\alpha = 0.0^\circ$

$\alpha = 20.0^\circ; \beta = -8.0^\circ \pm 1.0^\circ$

$\alpha = 40.0^\circ; \beta = -14^\circ \pm 1.0^\circ$

## UD-NCF



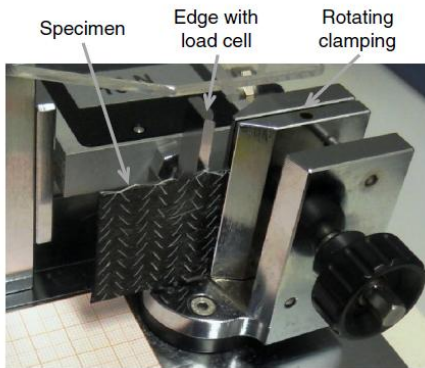
$\alpha = 0.0^\circ$

$\alpha = 20.0^\circ; \beta = 13^\circ \pm 1.0^\circ$

$\alpha = 40.0^\circ; \beta = 17^\circ \pm 1.0^\circ$

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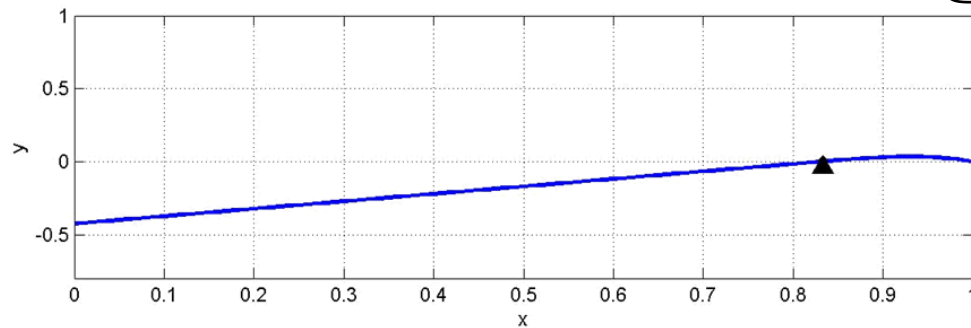


Beam theory (Timoshenko):

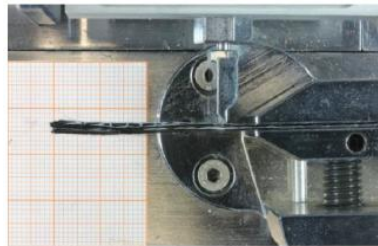
$$k = 1$$

$$\frac{dw(x)}{dx^2} = \frac{M(x)}{E \cdot I} - \frac{q(x)}{G^* \cdot A}$$

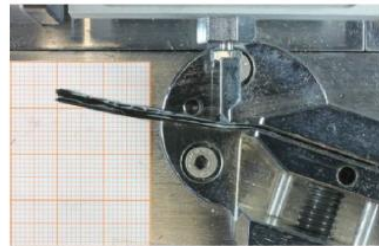
$$G^* = k \cdot G$$



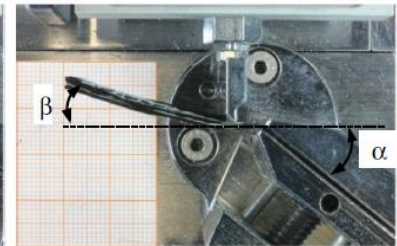
UD-NCF



$\alpha = 0.0^\circ$



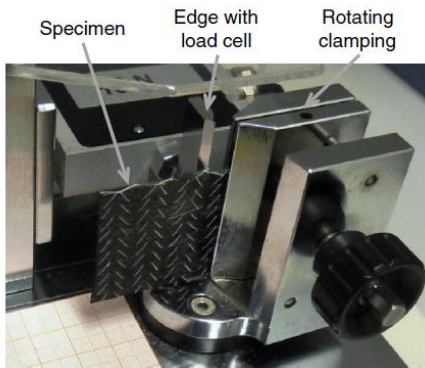
$\alpha = 20.0^\circ: \beta = 13^\circ \pm 1.0^\circ$



$\alpha = 40.0^\circ: \beta = 17^\circ \pm 1.0^\circ$

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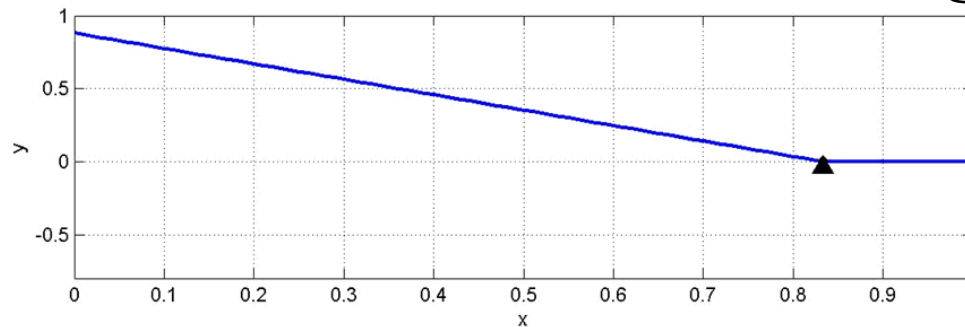


Beam theory (Timoshenko):

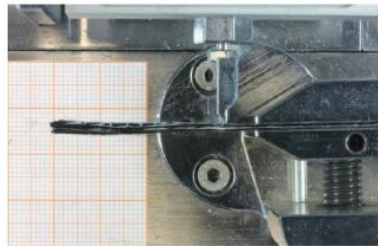
$$k = 1e-006$$

$$\frac{dw(x)}{dx^2} = \frac{M(x)}{E \cdot I} - \frac{q(x)}{G^* \cdot A}$$

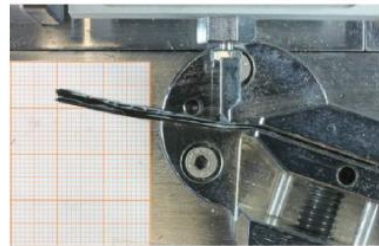
$$G^* = k \cdot G$$



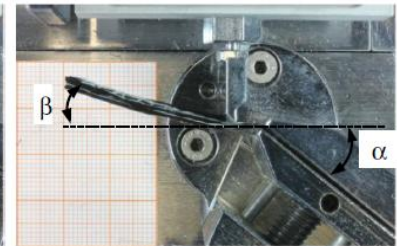
## UD-NCF



$\alpha = 0.0^\circ$



$\alpha = 20.0^\circ: \beta = 13^\circ \pm 1.0^\circ$

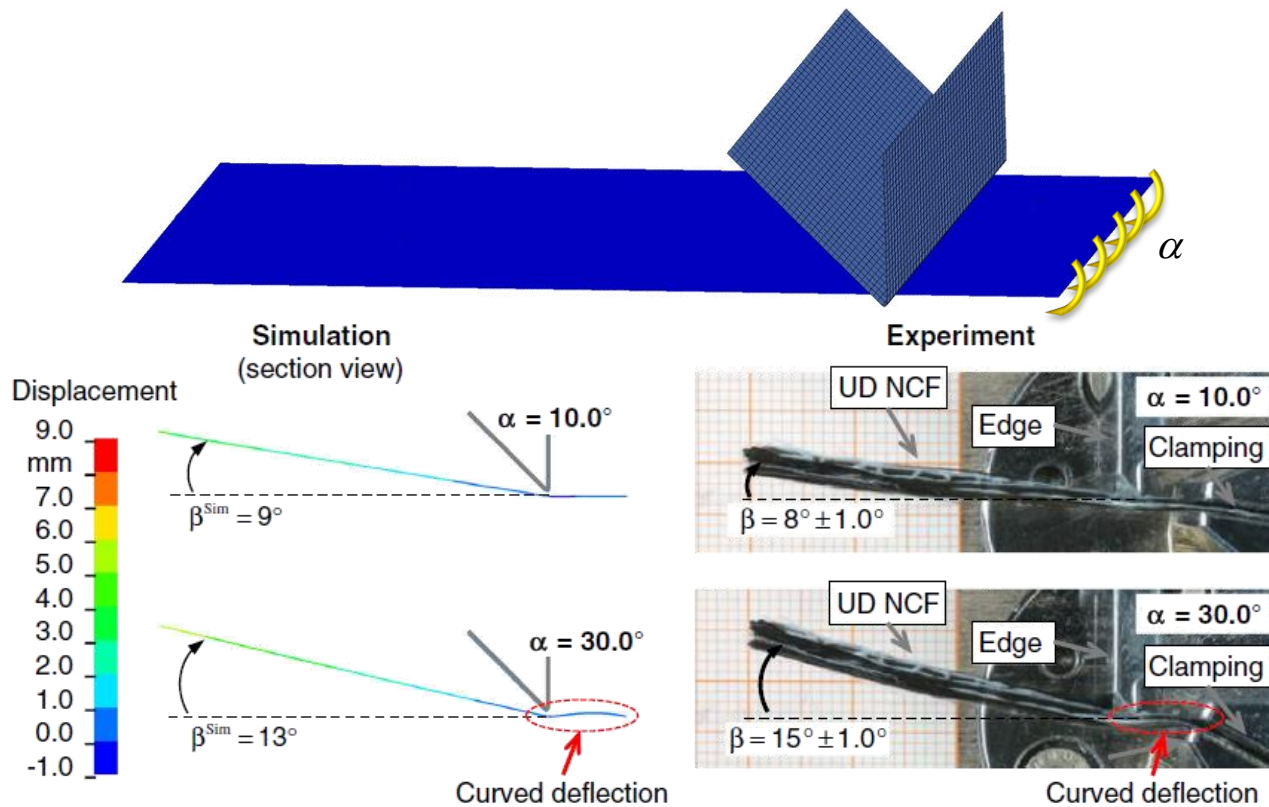


$\alpha = 40.0^\circ: \beta = 17^\circ \pm 1.0^\circ$

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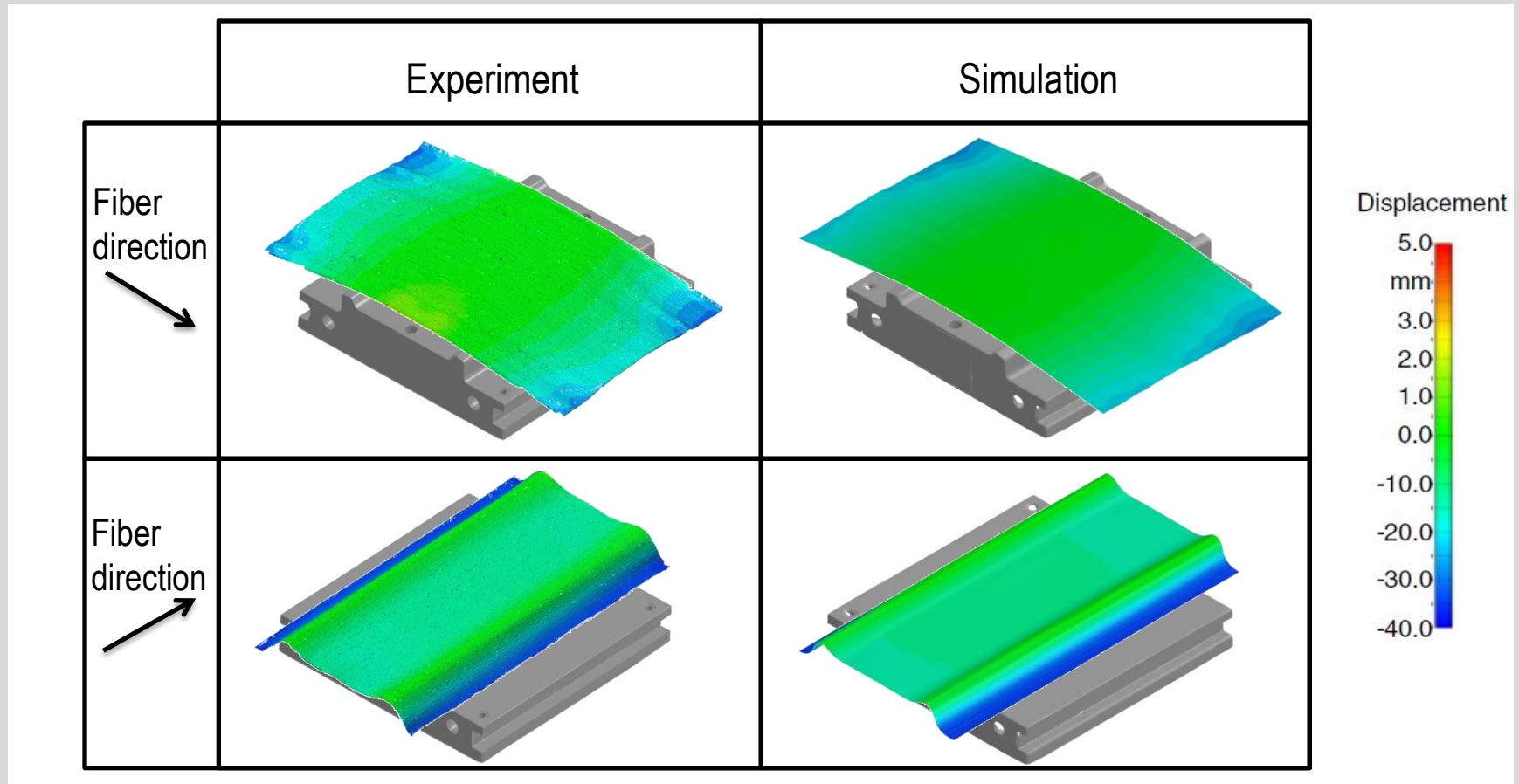
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## Calibration.



T. Senner et al.: Bending of unidirectional non-crimp-fabrics: experimental characterization, constitutive modeling and application in finite element simulation, Production Engineering Research and Development, DOI 10.1007/s11740-014-0568-5, pp 1-10.

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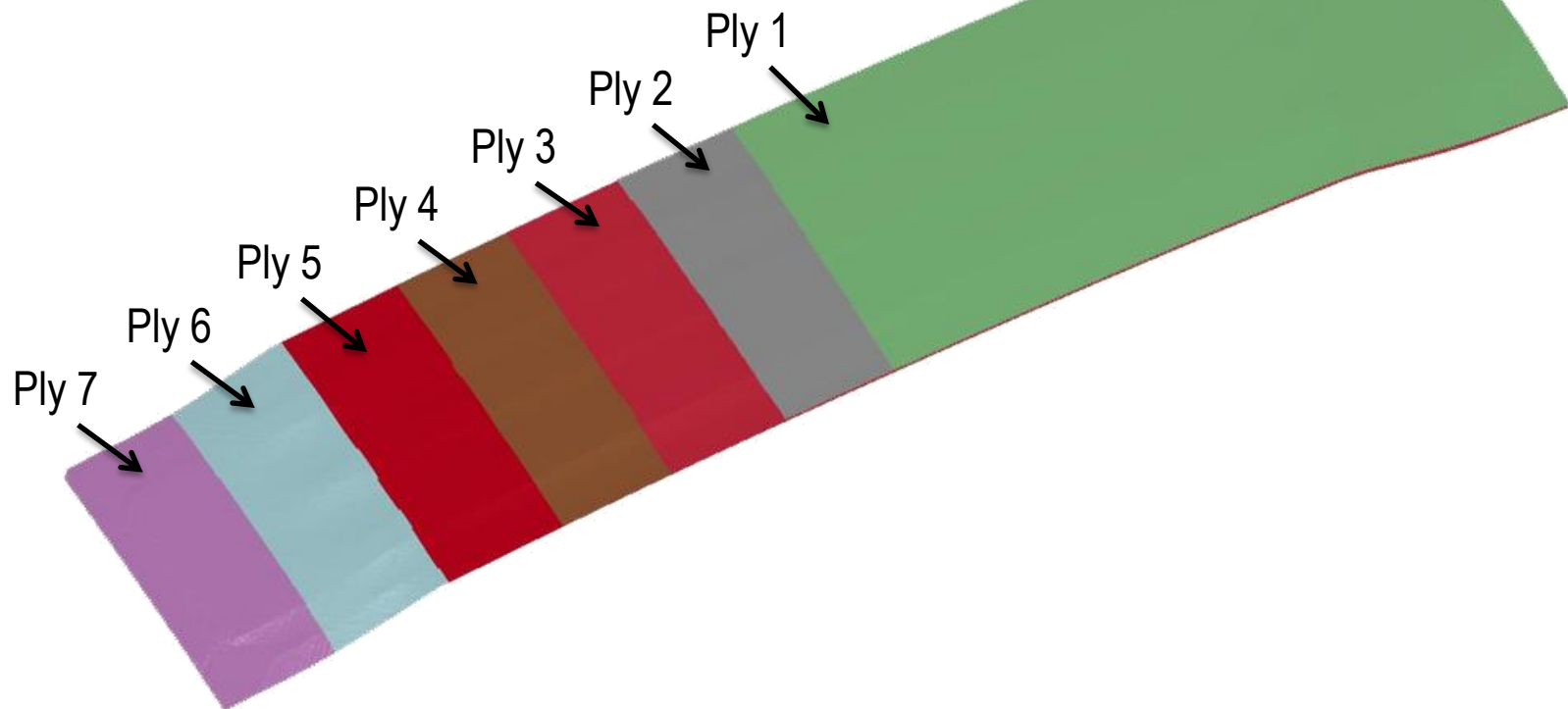


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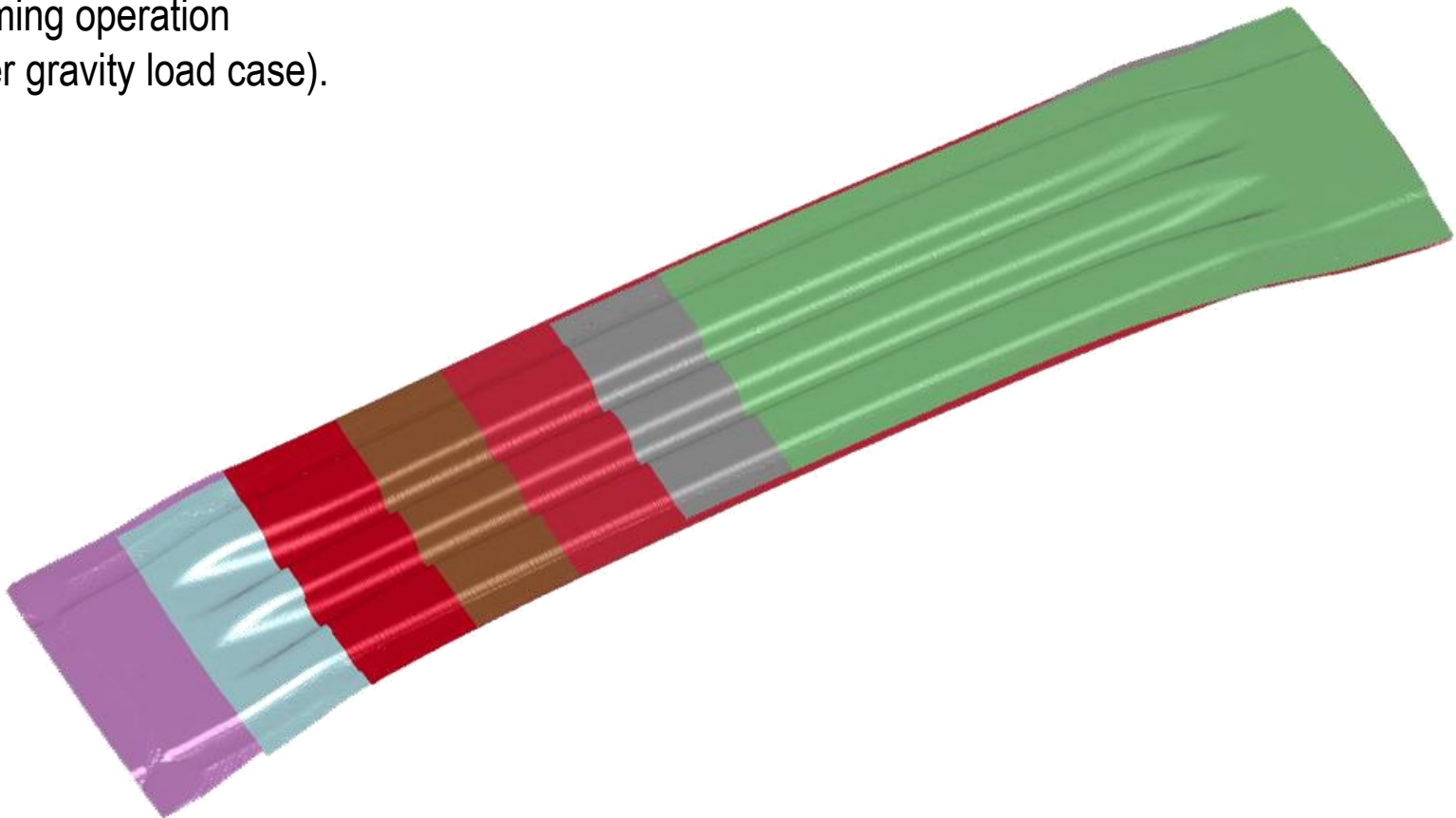
# SIMULATION RESULTS FOR PROTOTYPE PART. PLIES 1-7.

Forming operation  
(after gravity load case).

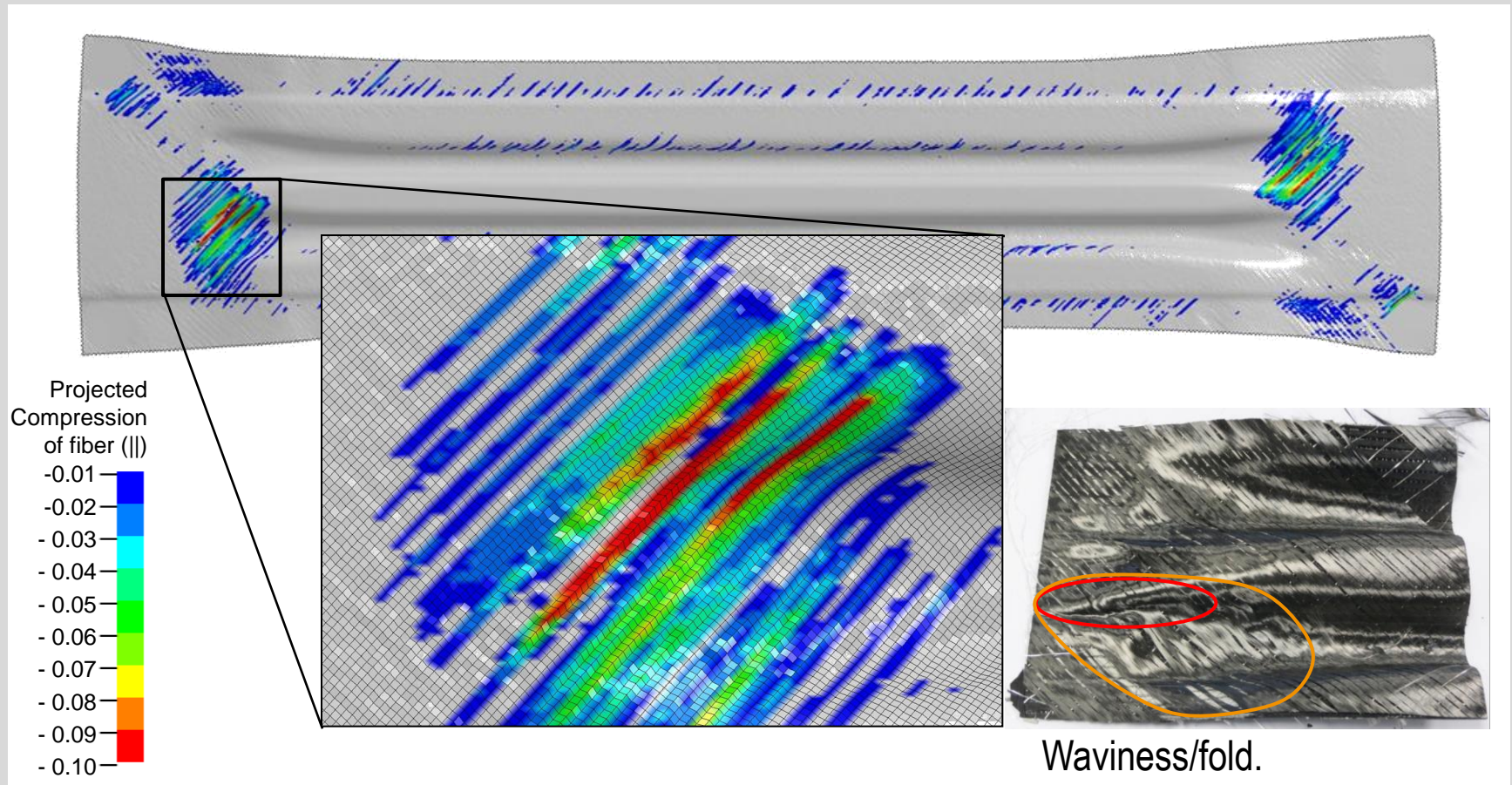


# SIMULATION RESULTS FOR PROTOTYPE PART. PLIES 1-7.

Forming operation  
(after gravity load case).



# SIMULATION RESULTS FOR PROTOTYPE PART. DETAIL: -45° PLY.



# LITERATURE.

T. Senner, S. Kreissl, M. Merklein, M. Meinhardt, A. Lipp (2014):  
*A modular modeling approach for describing the in-plane forming behavior of unidirectional non-crimp-fabrics*, Production Engineering Research and Development, DOI 10.1007/s11740-014-0561-z, pp 1-9.

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THANK YOU FOR YOUR ATTENTION.

